



U.S. MAGNET
DEVELOPMENT
PROGRAM

Nb₃Sn Magnets: 16-17 T dipole design studies

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- Target parameters
- Parametric model
- 60-mm aperture 16 T dipole
- Large aperture dipoles
 - 120-mm 2-layer design
 - 120-mm 4-layer design
- Requirements to the Utility Structure



16 T dipole target parameters

1. Geometrical
 - Magnet total length <2 m
 - Magnet straight section >200 mm
 - Free coil aperture 50 mm
 - Maximum magnet OD (reference number) 620 mm (FNAL/1.9K), 660 mm (BNL/1.9K), 914 mm (LBNL/4.5K)
2. Conductor
 - Strand diameter 0.7-1.2 mm
 - Cu:nonCu ratio 1.0±0.1
 - Non Cu $J_c(16T, 4.2 K)$ 1300 A/mm²
 - **RRR** >60
 - Reference $J_c(B, T)$ fit see below
 - I_c degradation due to cabling 5%
 - Maximum number of strands in cable 42 (FNAL), 60 (LBNL)
3. Operational
 - Reference temperature 1.9 K
 - Nominal operation field 16 T
 - Margin on the load-line @ 1.9K 10 % with respect to cable I_c
 - Geometrical field harmonics at $R_{ref}=17$ mm $b_n < 3$ for $n < 10$ (magnet straight section)
 - Target design field 17 T
 - Maximum coil stress 180 MPa (150 MPa during assembly)
 - Maximum coil-pole separation @ 17 T <10 μ m for cable width <50%
4. Quench protection
 - Maximum hot spot temperature 350 K
 - Total time delay 40 ms
 - Maximum voltage to ground @ quench 1.0 kV
 - Ground insulation design voltage >5 kV
5. Reference $J_c(B, T)$ fit:

$$B_{c2}(T) = B_{c20}(1 - t^{1.52}), J_c = \frac{C(t)}{B_p} b^{0.5}(1 - b)^2, C(t) = C_0(1 - t^{1.52})^{0.96}(1 - t^2)^{0.96}$$
 where $t=T/T_{c0}$; $b=B_p/B_{c2}(t)$, B_p is the conductor peak field, $T_{c0} = 16$ K, $B_{c20} = 29.4$ T, $C_0 = 270$ T·kA/mm².
6. Each magnet concept should provide
 - Description of magnet design including
 - Strand, cable and insulation (before and after reaction)
 - Coil cross-section (number of layers, number of turns, conductor weight/m/aperture)
 - Coil end design concept
 - Magnet support structure including transverse and axial support
 - Quench protection system in the case of no energy extraction
 - Maximum magnet bore field B_{max} at conductor SSL for 1.9 K and 4.5 K
 - Dependence of B_{max} on conductor $J_c(16T, 4.2K)$
 - Calculated geometrical field harmonics, coil magnetization and iron saturation effects in magnet straight section at $R_{ref}=17$ mm for $B=1-16$ T
 - Stress distribution in coil and structure at room and operation temperatures and at the nominal (16 T) and design (17 T) fields
 - Coil-pole interface (gap) at the nominal (16 T) and design (17 T) fields
 - Coil maximum temperature and coil-to-ground voltage during quench w/o energy extraction
 - **Cost reduction opportunities**

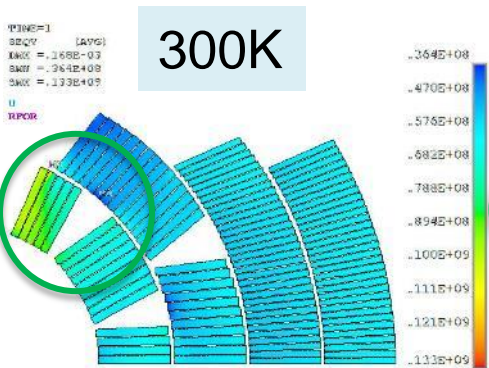
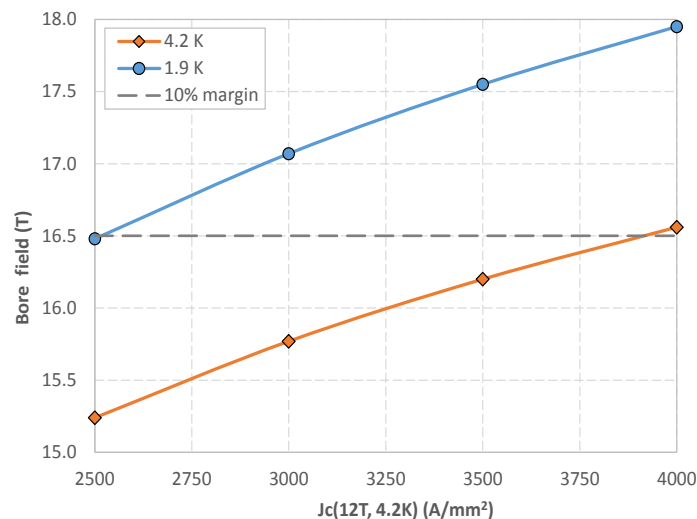
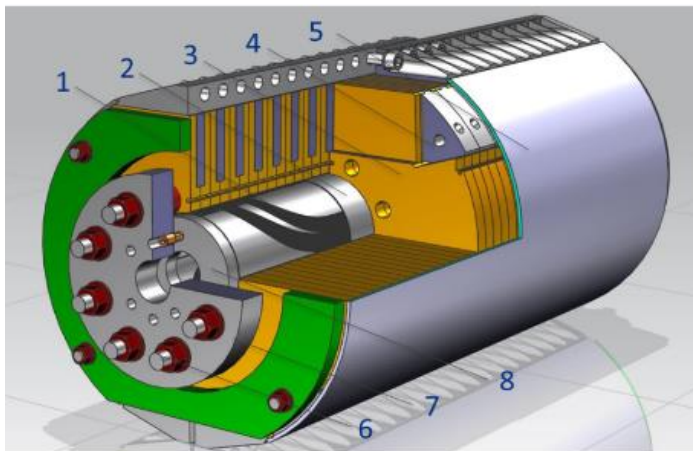
Target parameters has been formulated for the next MDP dipole model which will be fabricated and tested after the 15 T dipole demonstrator at FNAL and the CCT program at LBNL.

Timeline:

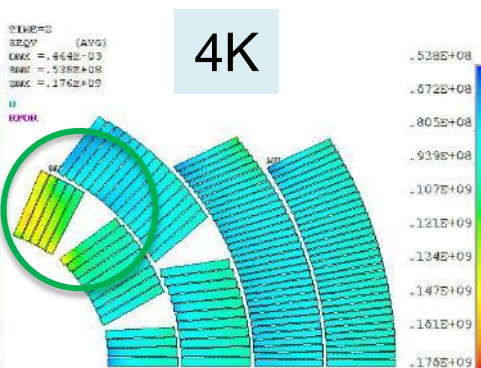
- Model fabrication in FY19+ per MDP plan.
- Engineering design and initial procurement FY18+
- Design studies and selection FY17+.



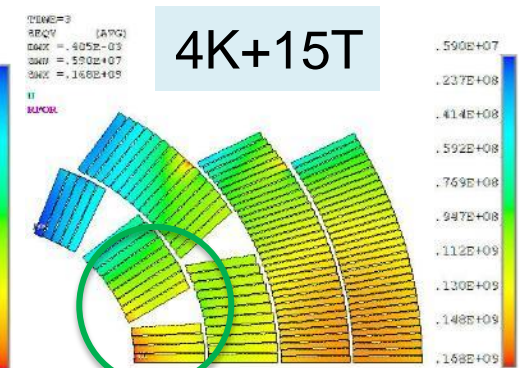
15 T dipole demonstrator: possibilities and limitations



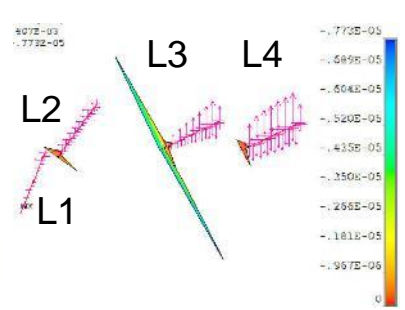
$S_{eqv} = 133 \text{ MPa}$



$S_{eqv} = 176 \text{ MPa}$

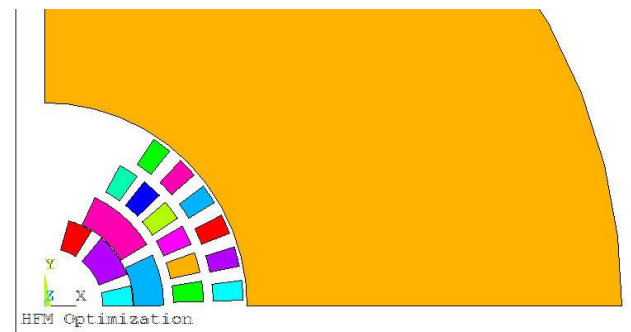
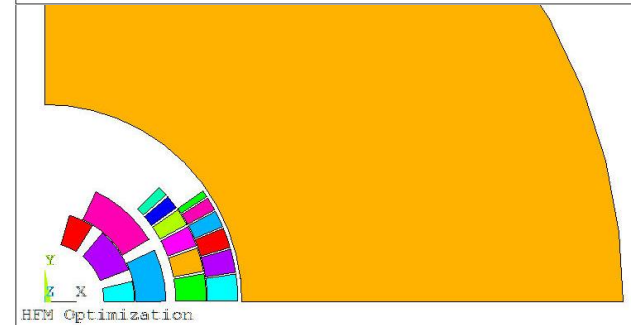
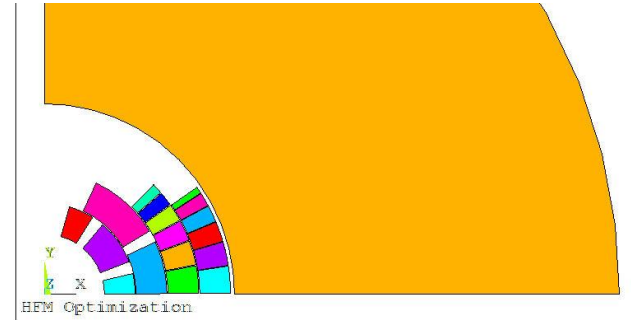
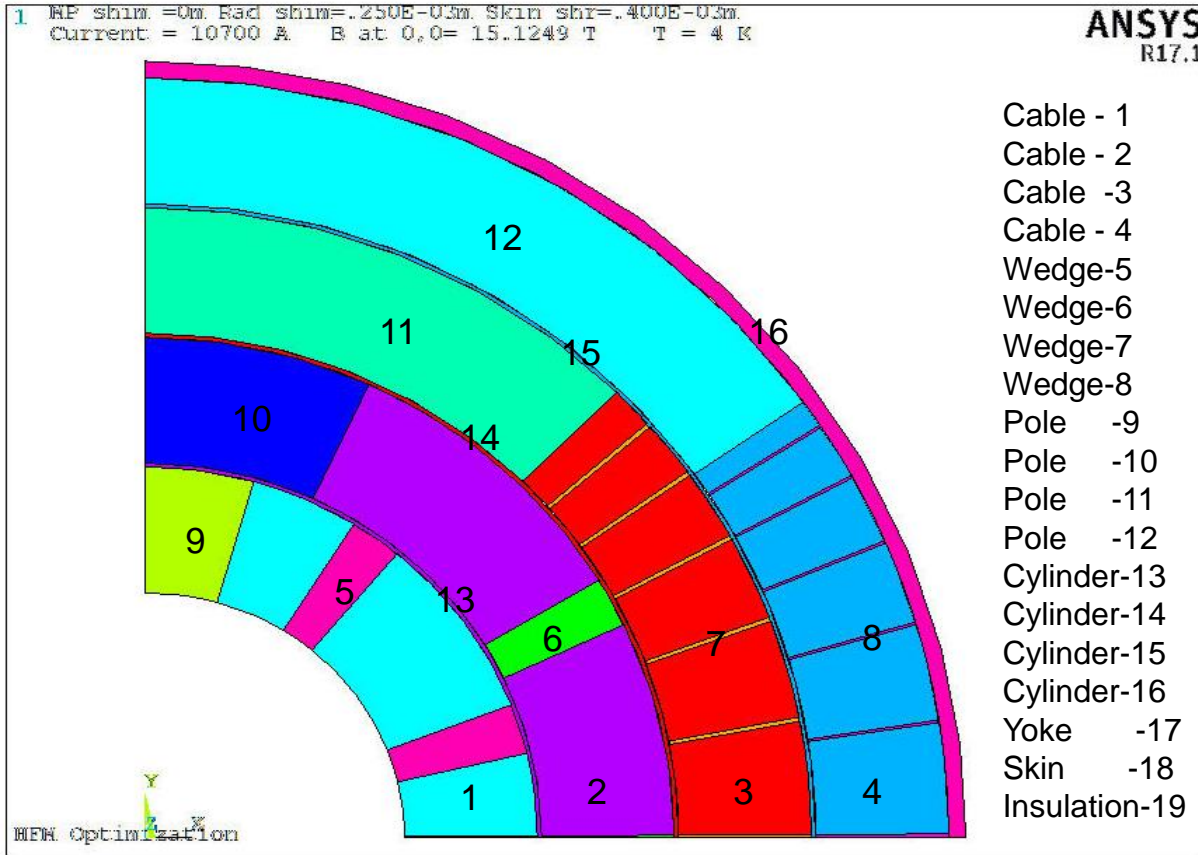


$S_{eqv} = 168 \text{ MPa}$





Parametric Model



- Radial shim for coil prestress
- Iron yoke is vertically split and closed

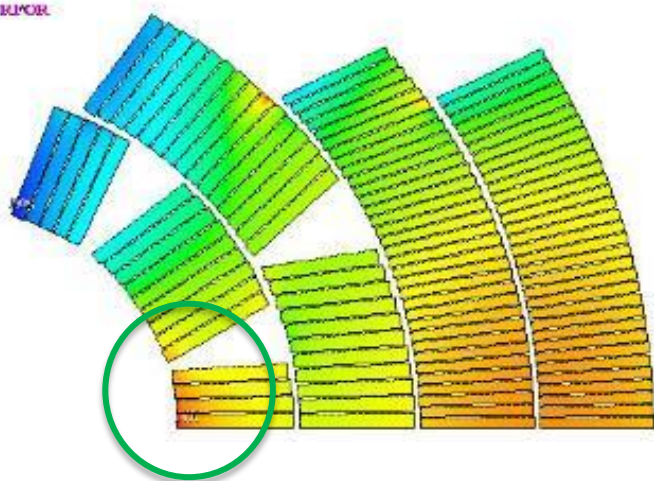


Model verification

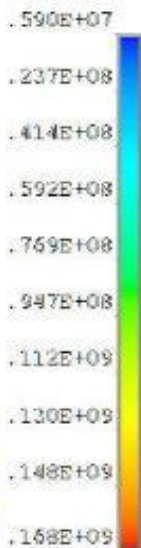
4K B=15T

TIME=3
SEQV (AVG)
MAX = .405E-03
SMN = .590E+07
SMX = .168E+09

$S_{eqv} = 168 \text{ MPa}$

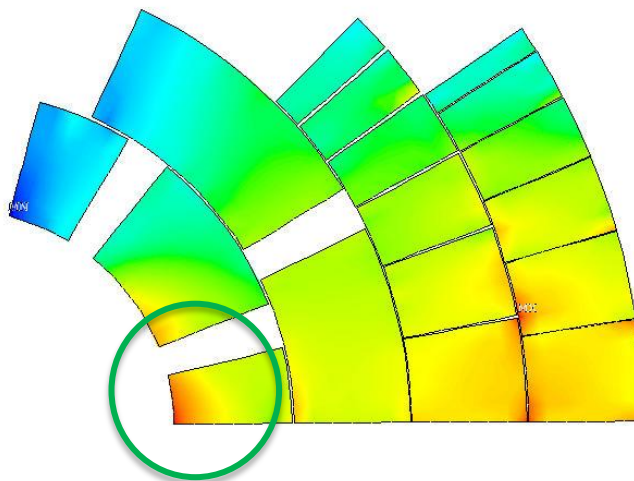


BL



1 MF SHM = 0m ESD SHM = .200E-03m SKIN SHM = .400E-03m
Current = 10700 A B at 0,0= 15.1249 T T = 4 K

$S_{eqv} = 164 \text{ MPa}$



SM

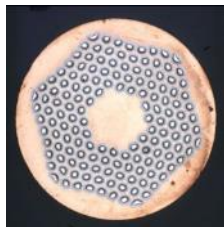
MF Optimization

ANSYS Release 17.1
Build 17.1
APR 30 2017
13:19:20
NODAL SOLUTION
STEP=3
SUB =1
TIME=3
SEQV (AVG)
PowerGraphics
EFACET=1
AVRES=Max
MAX = .405E-03
SMN = .350E+07
SMX = .164E+09
Color scale legend:
- .350E+07
- .135E+08
- .235E+08
- .335E+08
- .435E+08
- .537E+08
- .637E+08
- .738E+08
- .838E+08
- .938E+08
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- .134E+09
- .144E+09
- .154E+09
- .164E+09

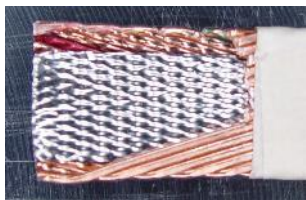


Cable parameters

RRP-108/127
0.7 mm



RRP-150/169
1 mm

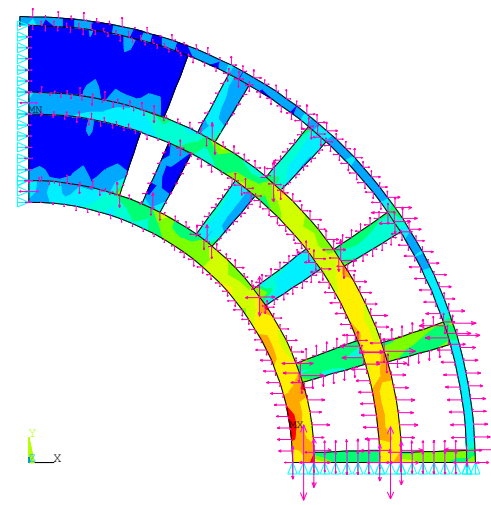
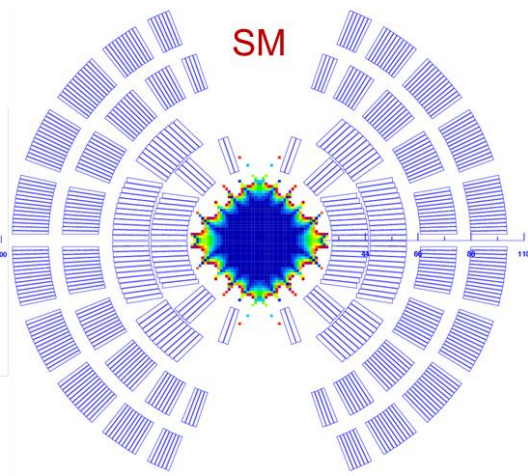
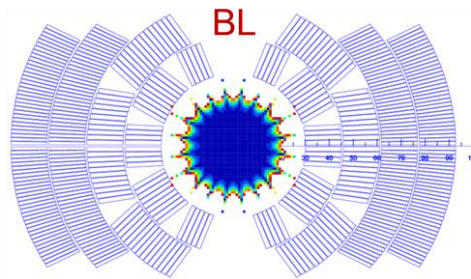


- Both BL and SM coils use the same cables in the inner and outer coils.

Parameter	Inner Coil	Outer Coil
Number of strands	28	40
Mid-thickness, mm	1.870	1.319
Width, mm	15.10	
Keystone angle, deg.	0.805	
Cu/nonCu ratio	1.13	
$J_c(15T, 4.2K), A/mm^2$	1500	

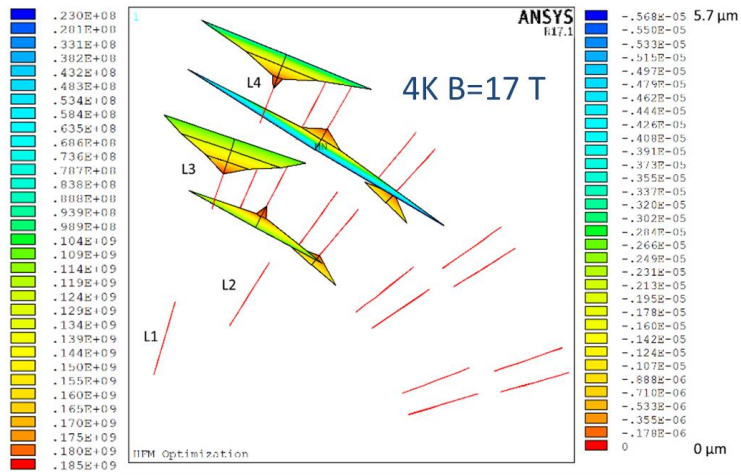
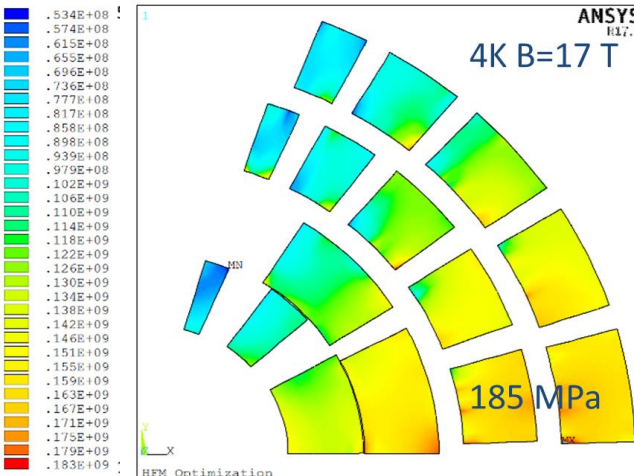
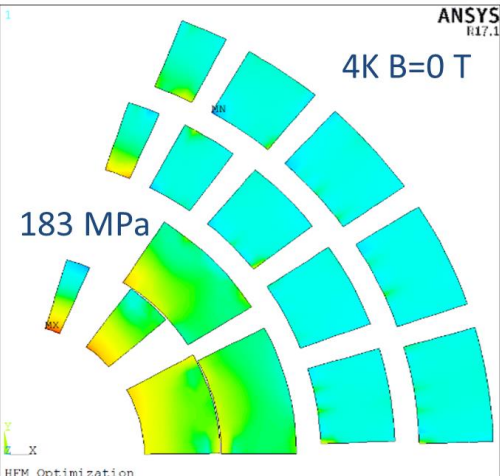
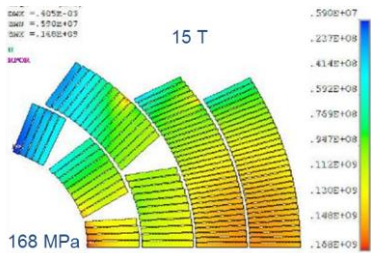


60-mm aperture 16 T dipole with SM



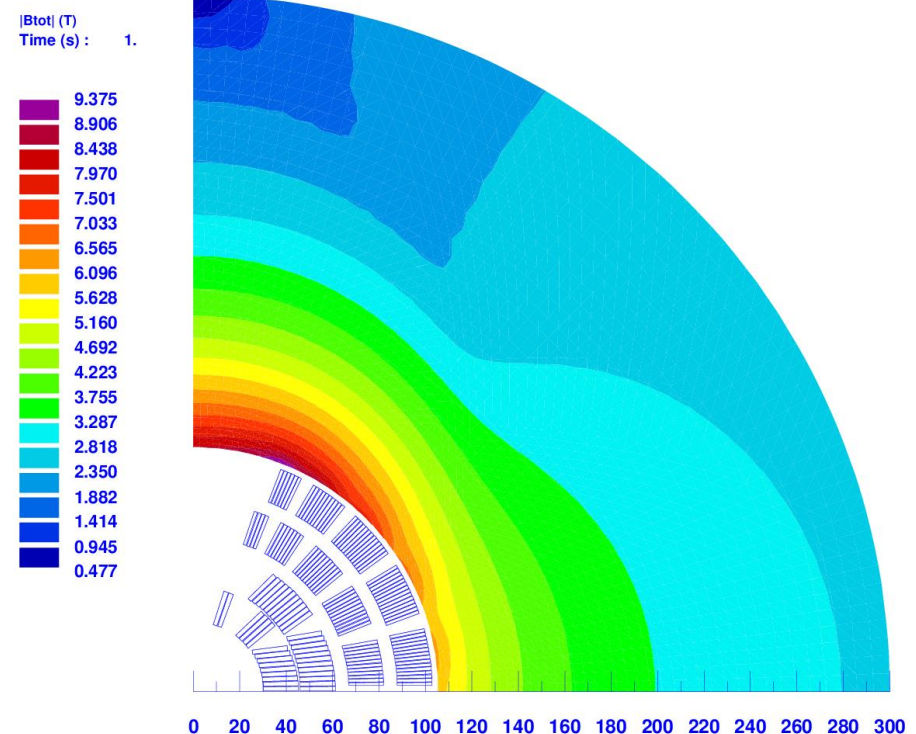
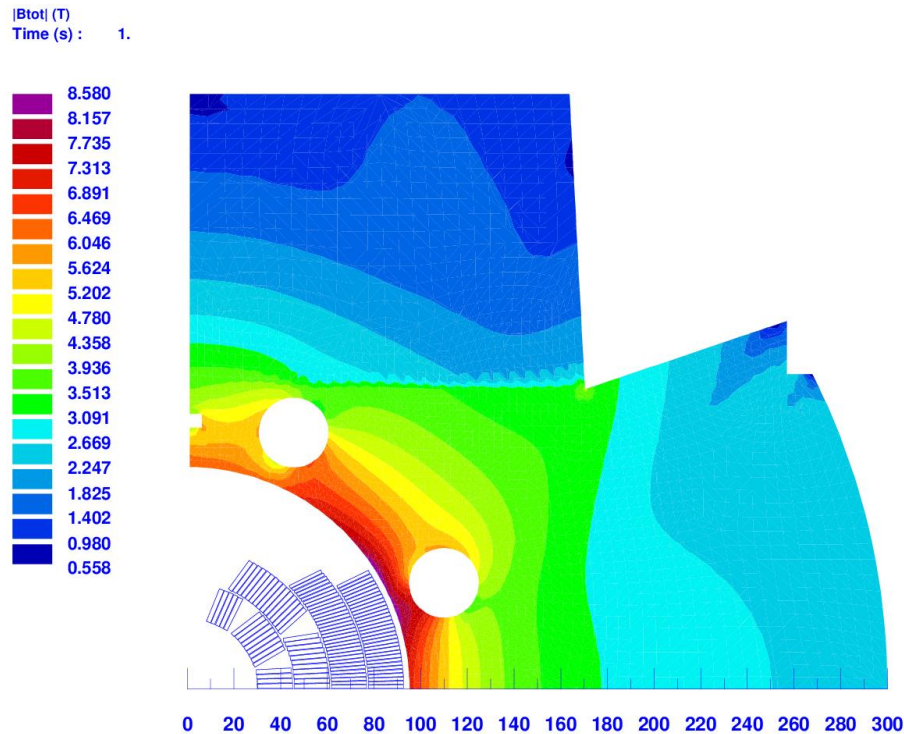
ANSYS Release
Build 17.1
U
NFOR
RFOR

Blue	.992E+07
Light Blue	.585E+08
Cyan	.107E+09
Green	.156E+09
Yellow-Green	.204E+09
Yellow	.253E+09
Orange	.302E+09
Red-Orange	.350E+09
Red	.399E+09
Dark Red	.447E+09
Black	.496E+09





Iron yoke

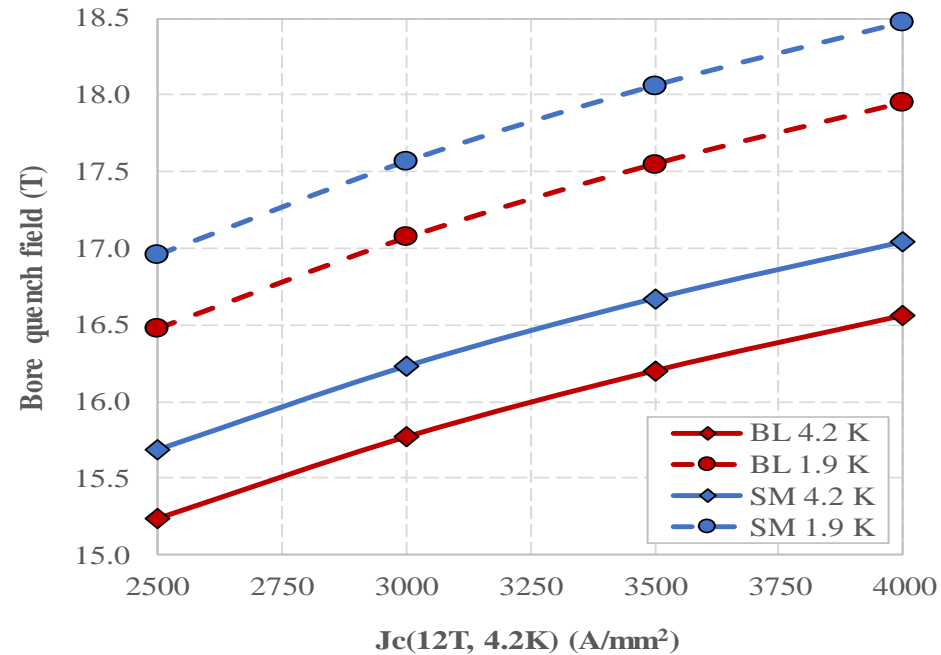


- The model included a cylindrical iron yoke with the outer diameter of 600 mm and non-linear magnetic properties for the purpose of field calculation.
- The yoke design is to be optimized based on the structural analysis.



Magnet parameters

Parameter	BL		SM	
	IC	OC	IC	OC
Bore field, T	15.61		16.07	
Peak field, T	16.25		16.44	
Current, A	11.34		10.80	
Inductance, mH/m	25.61		35.42	
Stored energy, MJ/m	1.65		2.06	
F_x , MN/m/quadrant	5.8	1.6	4.8	4.7
F_y , MN/m/quadrant	-1.2	-3.3	-0.5	-3.6
Number of turns	44	65	38	102



- SM design has 30% more turns, larger inductance and stored energy.
- The horizontal Lorentz force per the inner coil is a factor of 1.2 smaller and the vertical force is a factor of 2.4 smaller than in the BL design.
- The horizontal force on the outer SM coil is a factor of 3 higher than that for the outer BL coil, while the vertical force is practically the same.



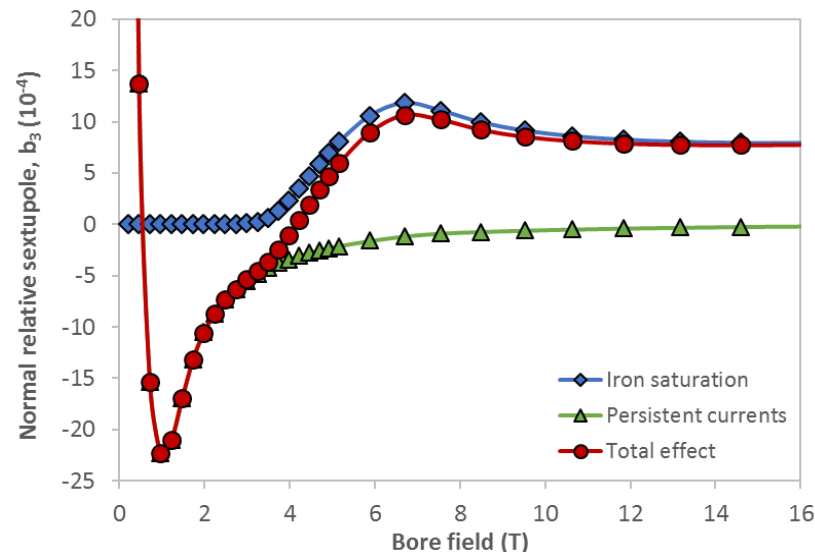
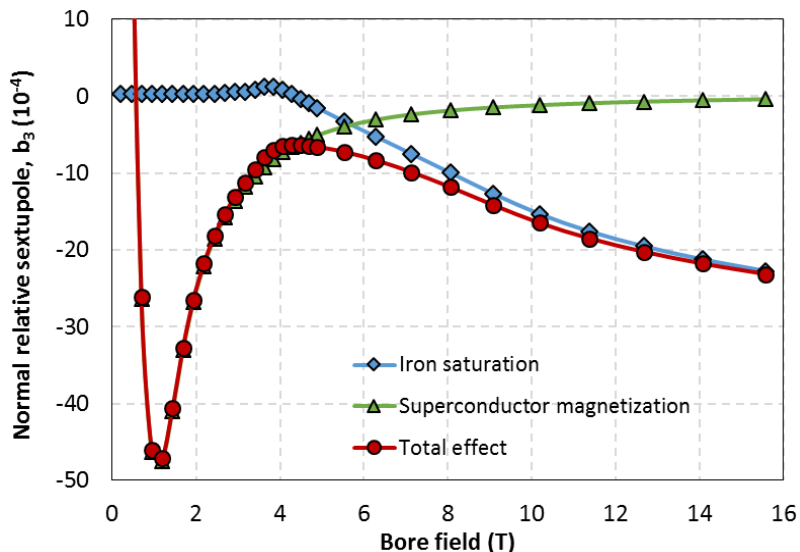
Field quality

Table 2: Geometrical harmonics at $R_{ref}=17\text{mm}$ (10^{-4})

Harmonic	BL	SM
b_3	0.0018	0.0007
b_5	0.0154	-0.0087
b_7	0.0523	0.1170
b_9	0.0612	0.2626
b_{11}	0.3433	-0.0873

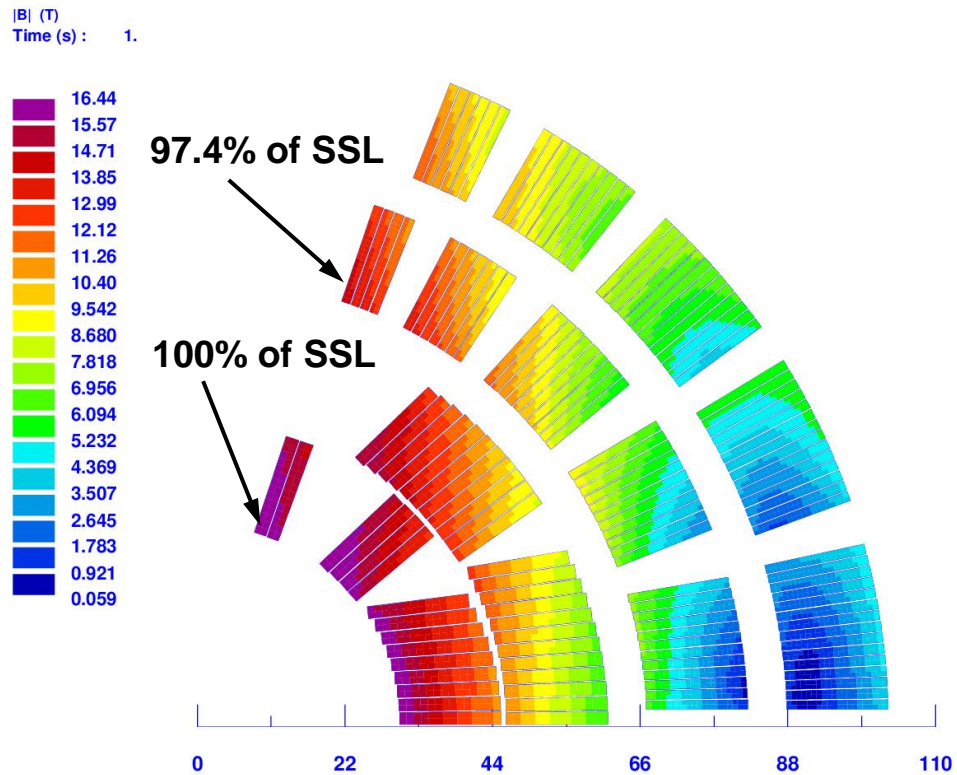
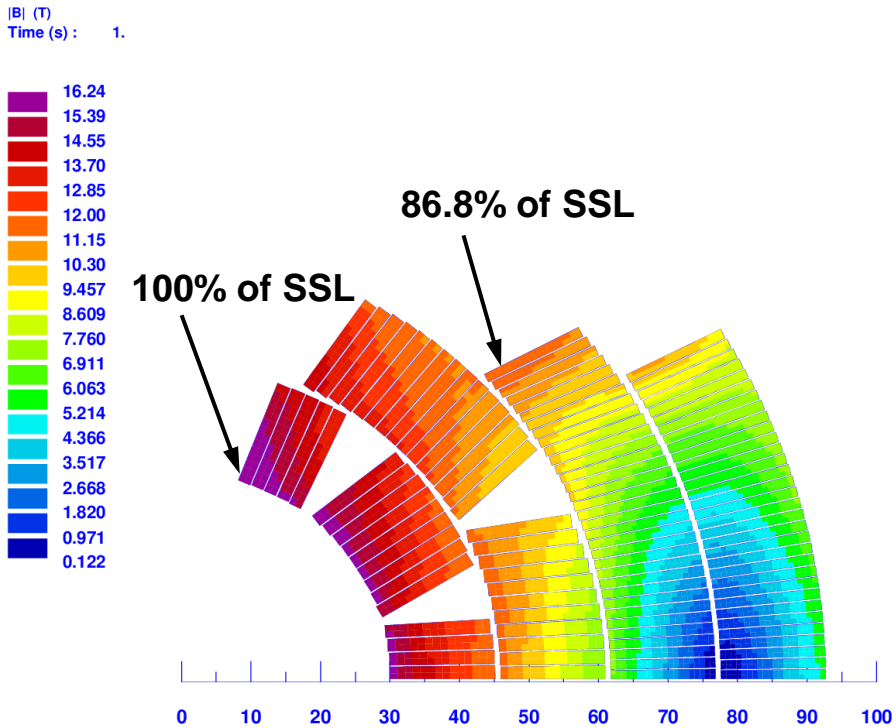
- Both designs provide the geometrical field quality better than 10^{-4} at $R_{ref}=17\text{mm}$.
- There is a noticeable difference in the iron saturation and coil magnetization effects

○ b_3 variation is reduced by a factor of ~ 2 .



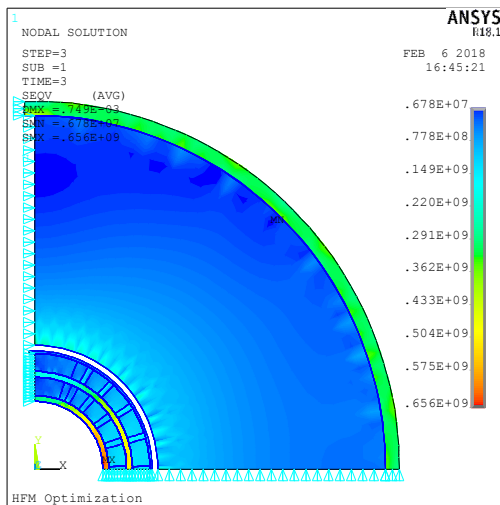


Coil fields and margins

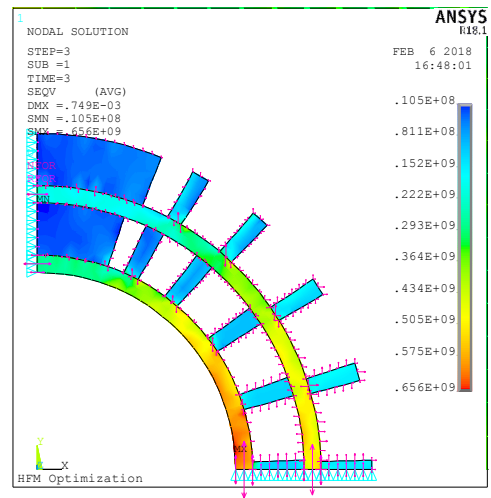
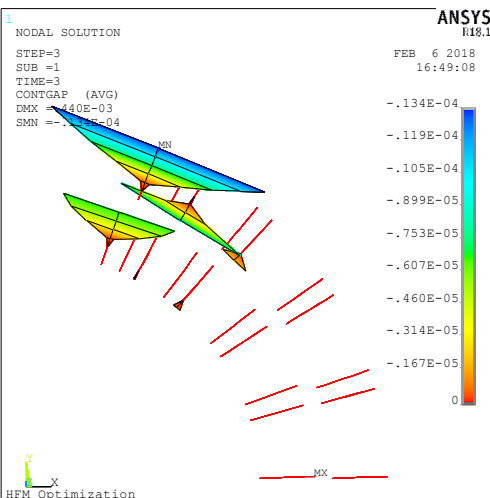
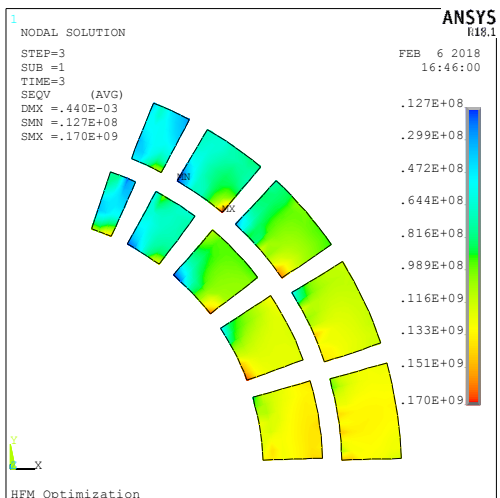




120 mm 2-layer dipole

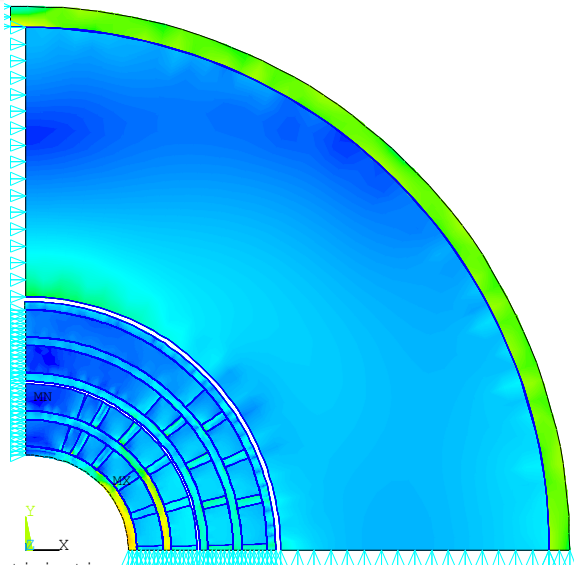


I kA	B T	Scoil MPa	Pole Gap μm	Ssup MPa
12	11.0	170	16	556
14	12.5	203	50	611
16	14.0	256	90	688

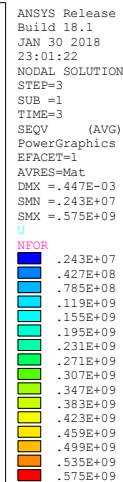
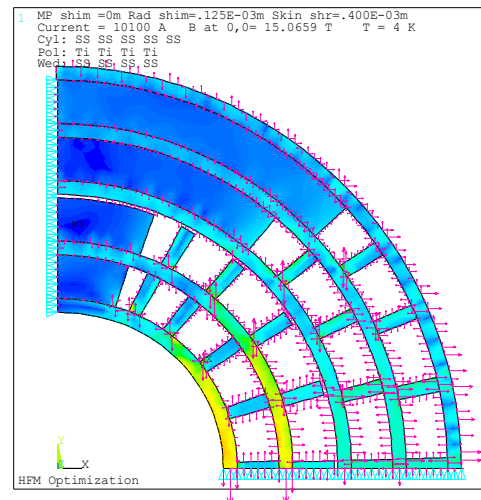
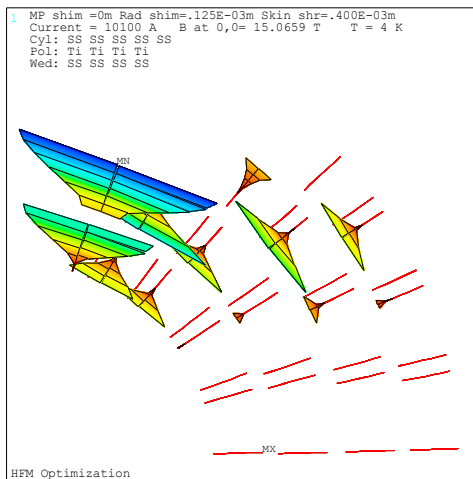
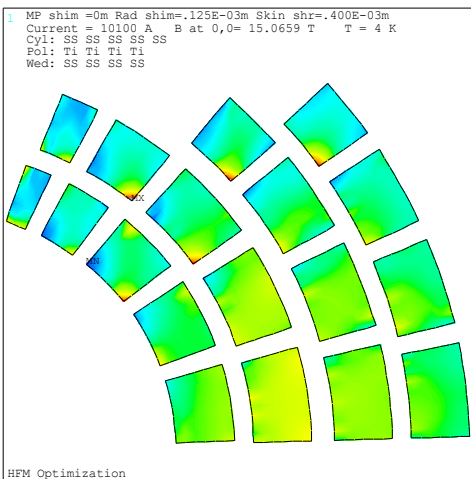




120-mm aperture 15 T dipole

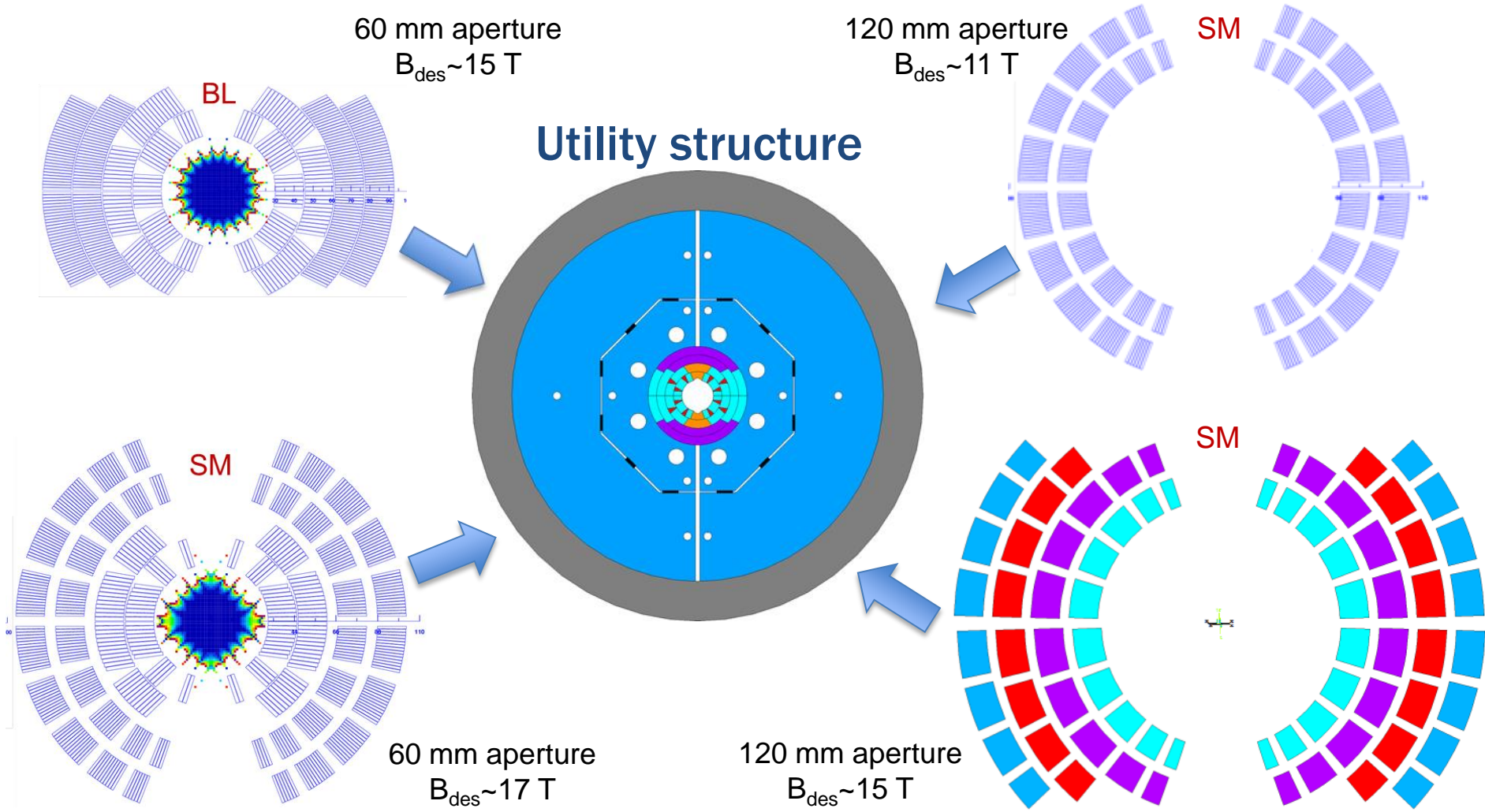


I kA	B T	Scoil MPa	Pole gap μm	Ssup MPa
10.1	15	190	24	575
10.8	16	200	50	637
11.6	17	210	90	699



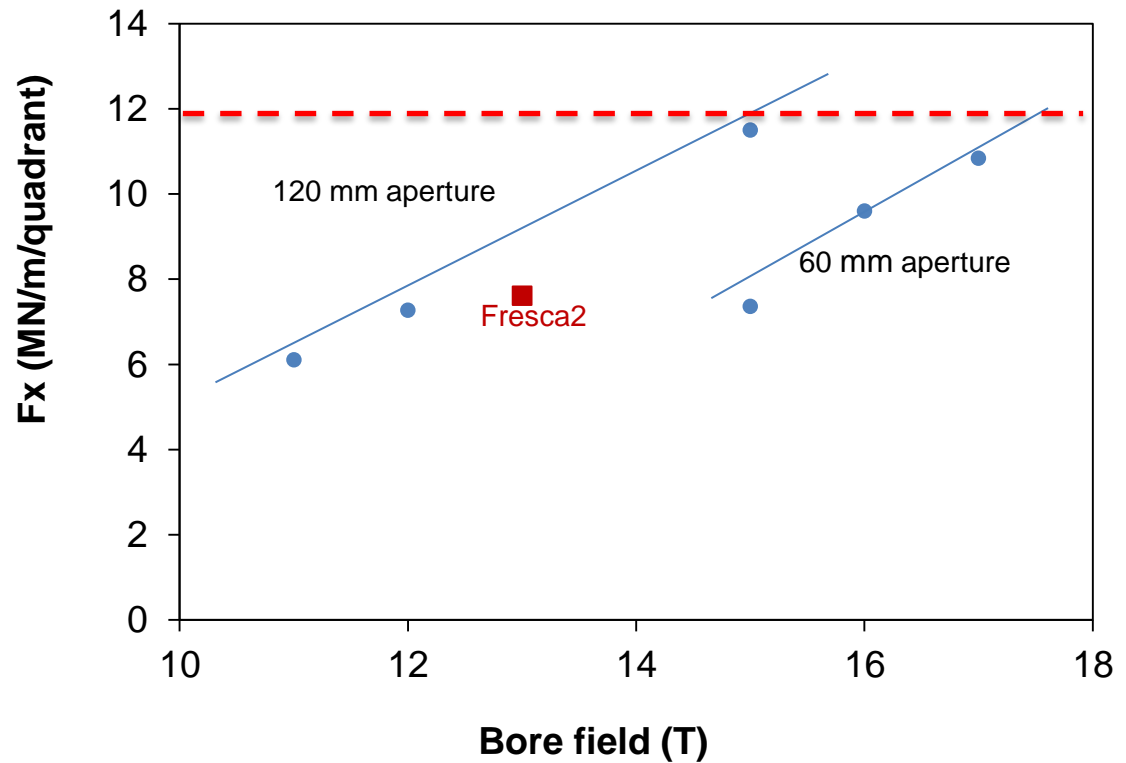
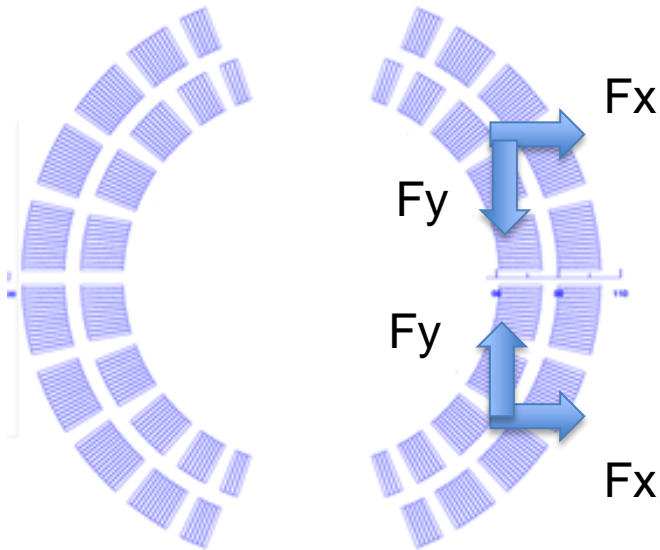


Cos-theta dipole sequence





Horizontal force



- Support structure has to keep iron yoke closed



- **60-mm 4-layer dipole design with stress management meets the design parameters of MDP Step 3**
 - to be reviewed and approve before engineering design
- **120-mm 2-layer dipole based on two outer layers with stress management can provide design field up to 11-12 T**
 - technological model to study stress management in cos-theta coils
 - outsert to test HTS coils
- **120-mm 4-layer dipole with stress management can provide design fields up to 15 T**
 - can be used as outsert for hybrid dipole
 - study and optimization will continue