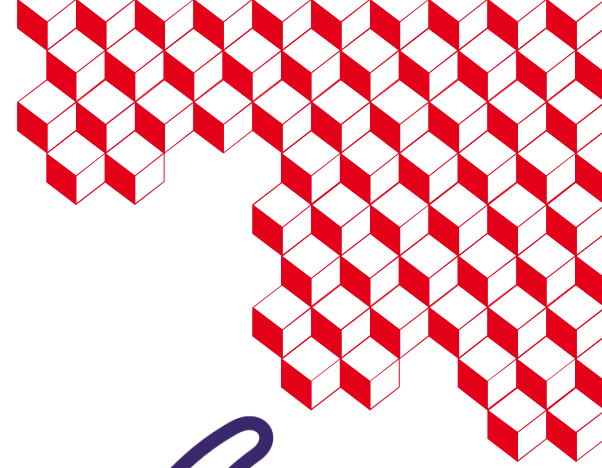




irfu



# NEWGAIN - ASTERICS

## Mini workshop LBNL/FRIB/CEA

### Cryogenic Design Overview

Damien Simon – Tanguy Cadoux – Elena Fernandez Mora

Hélène Felice – Bertrand Hervieu – Armand Sinanna – Hervé Allain

Roser Vallcorba – Christophe Berriaud – Francesco Stacchi

Robert Touzery – Sony Trieste – Thibault Genestier – Patrick Graffin

Thierry Guillo – Nicolas Bakon – Victor Kleymenov – David Vurpillot

Etienne Rochepault – Jean-Marc Gheller – Thomas Thuillier



# outline

1. Introduction
2. Cryogenic synoptic
3. Cryogenic Design
4. Condenser
5. Current leads
6. Thermal budget at 4 K
7. Thermal screen simulation
8. Cool down
9. Instrumentation
10. Conclusions

# 1. Introduction / magnet cooling



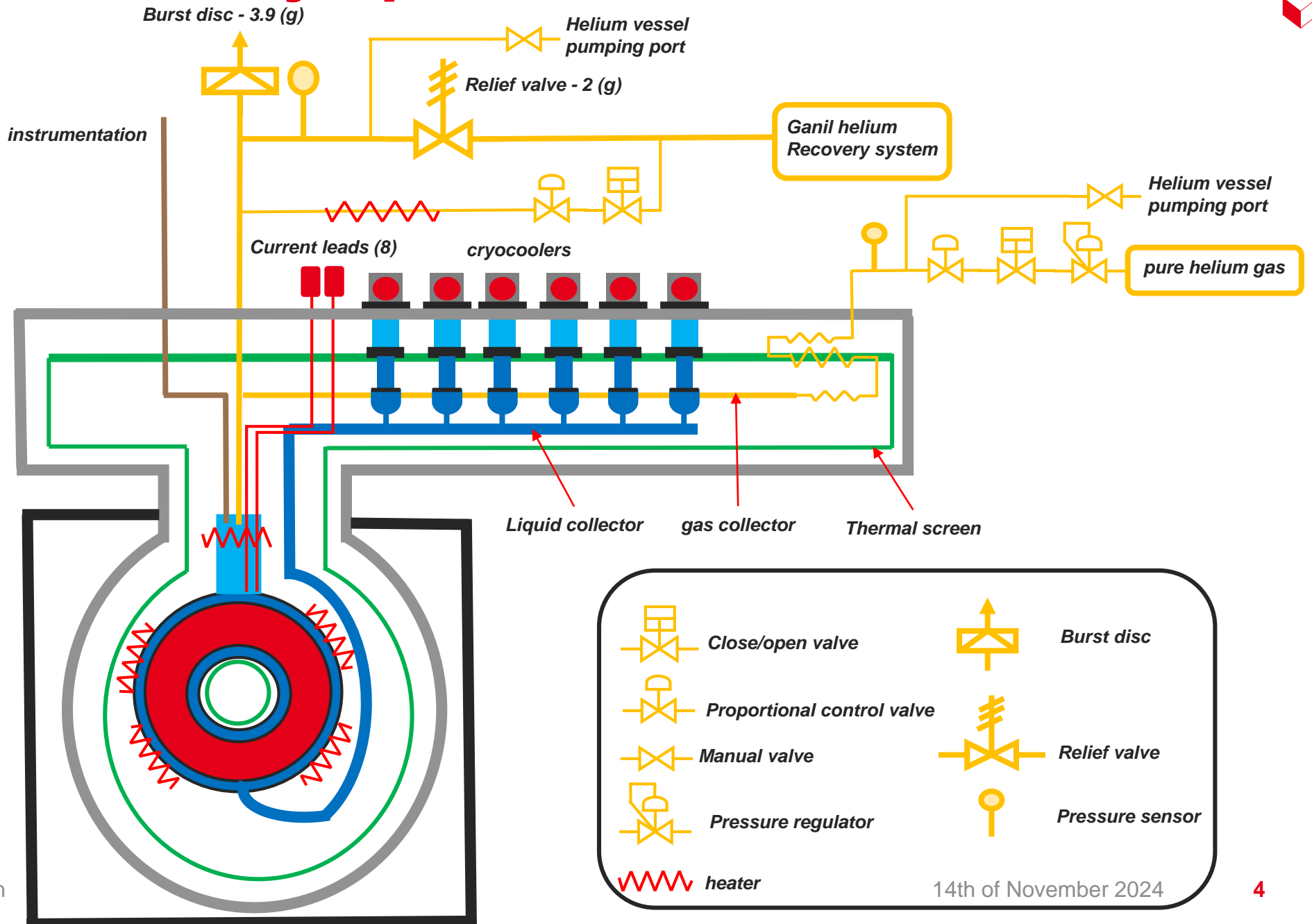
- Magnet immersed in a liquid helium bath – 1.1 bar, 4.31 K
- The different heat loads vaporize liquid helium
- Cold vapors liquefied by condensers connected to the second stage of cryocoolers
- Adjustment between cooling power and heat load by heaters that vaporize liquid
- Thermal shield circuit connected to the first stage of cryocoolers
- Heat loads: 7 W dynamic + static heat loads (radiation + conduction)
- HTS current leads
- PED: burst disc and valve to protect the system against over pressure

# 2. Magnet and satellite synoptic

❖ **Operating pressure**  
**1.1 bar**  
 ➤  $T_{\text{liquid}} = T_{\text{sat}} = 4.31 \text{ K}$

❖ **Operating modes**

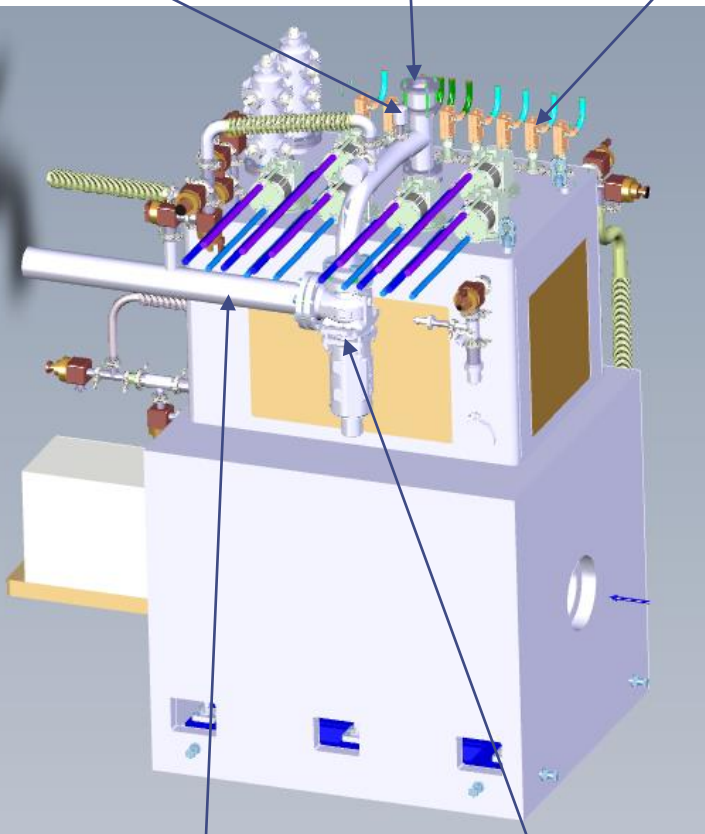
- Cool down
- Normal operation
- Quench
- Major default
- Warm up



# 3. Cryogenic design (1/3)

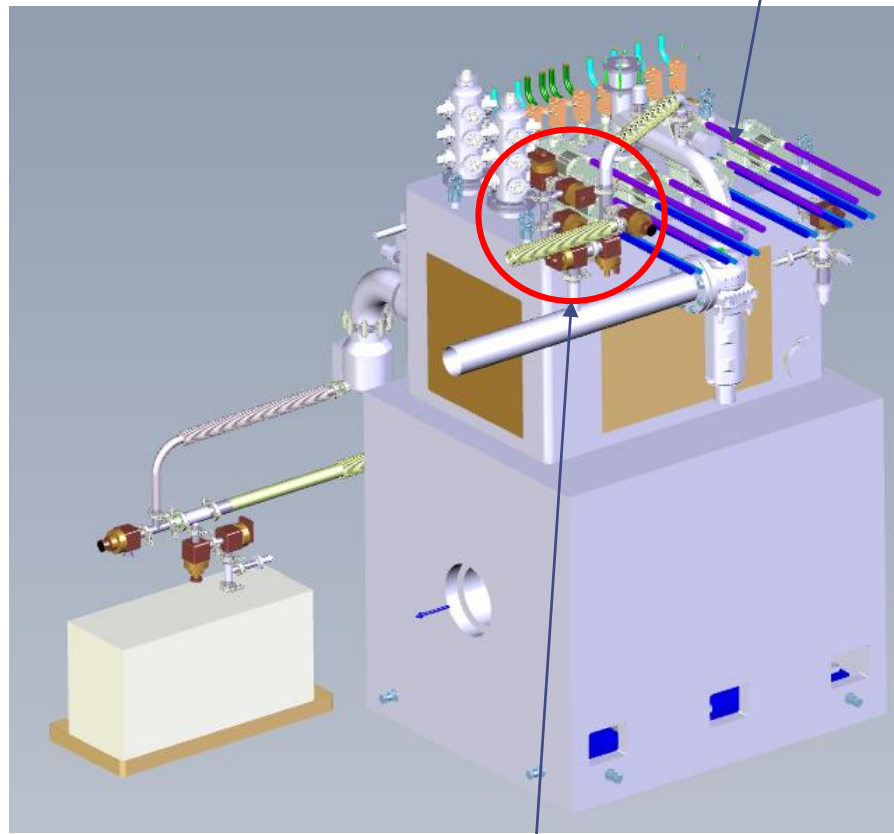


Anti-Taconis system  
Burst disc  
Current leads



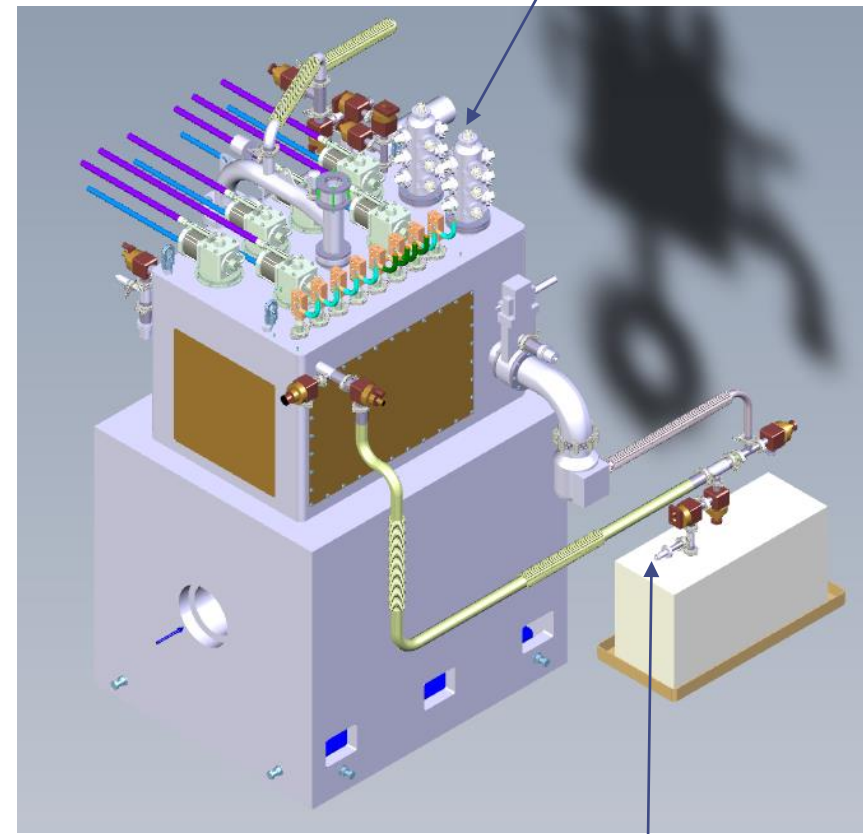
Helium recovery line  
Safety valve

cryocoolers



Helium feeding and pressure  
Regulation valves system

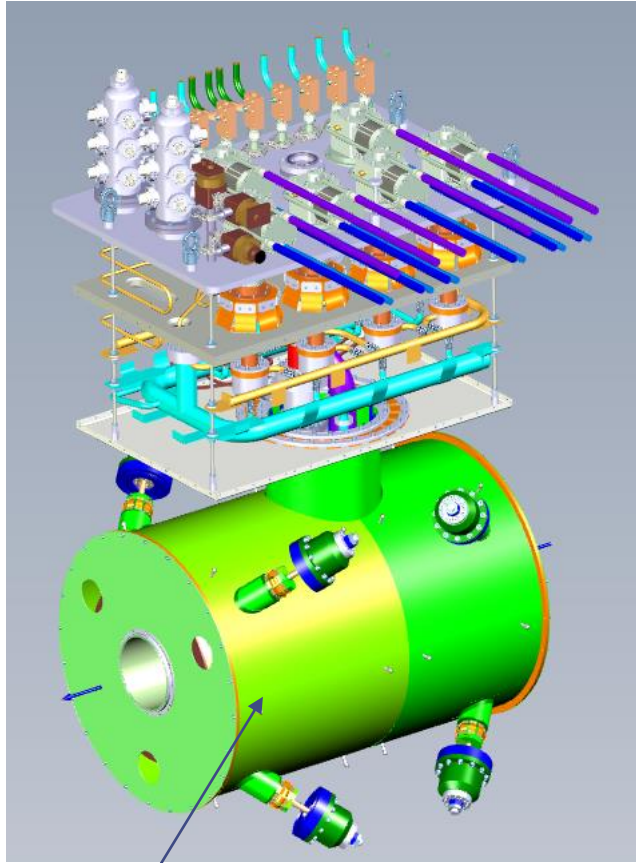
Instrumentation feedthrough



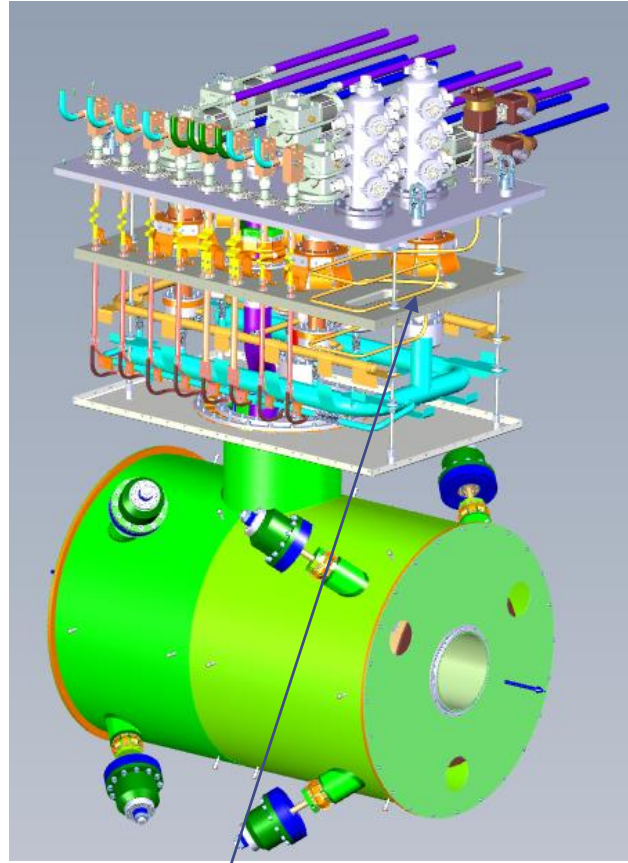
Vacuum pumping system



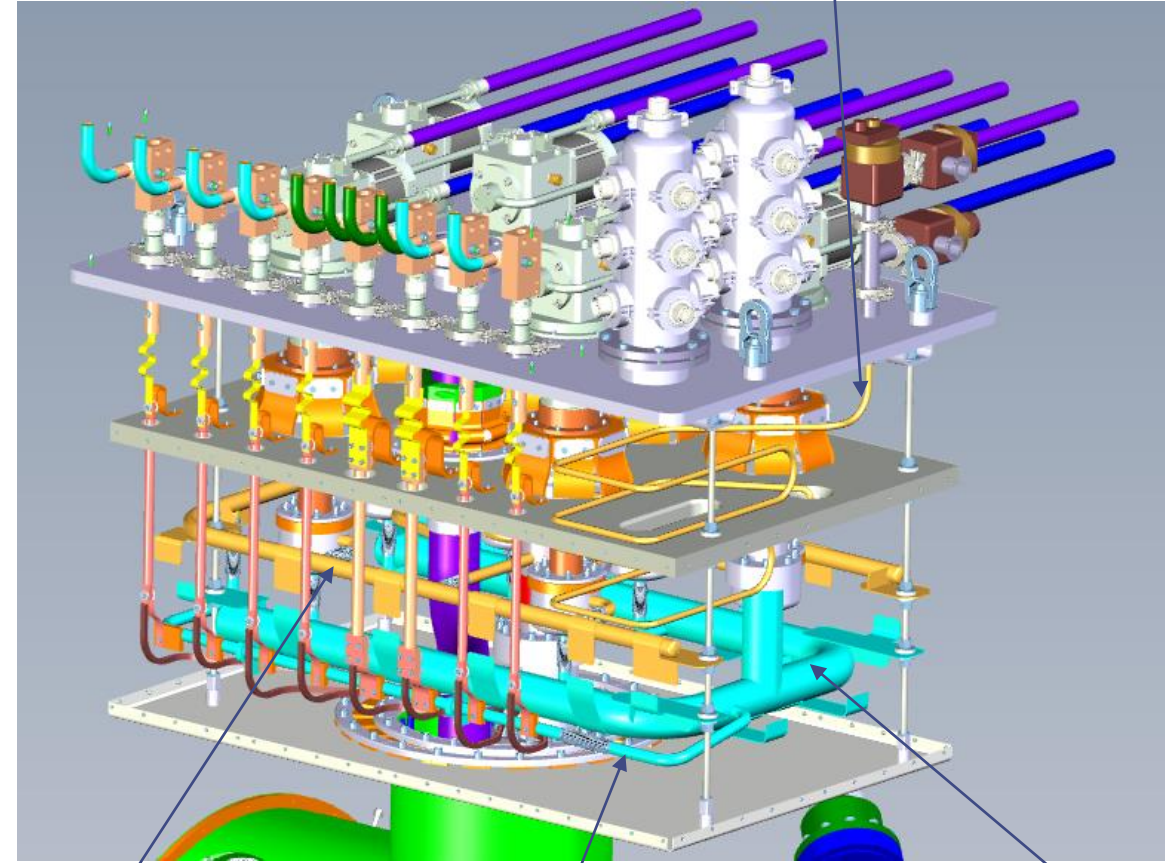
### 3. Cryogenic design (2/3)



Thermal shield



Thermal shield plate  
connected to first stage  
of cryocooler



Helium feeding pipe  
connected to gas collector

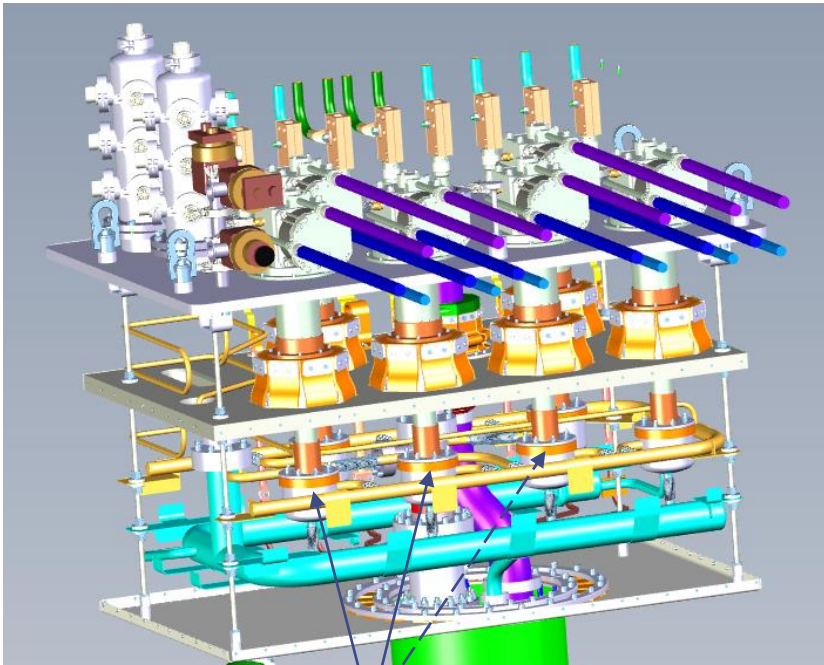
Gas collector

liquid helium tube  
to cool bottom of  
current leads

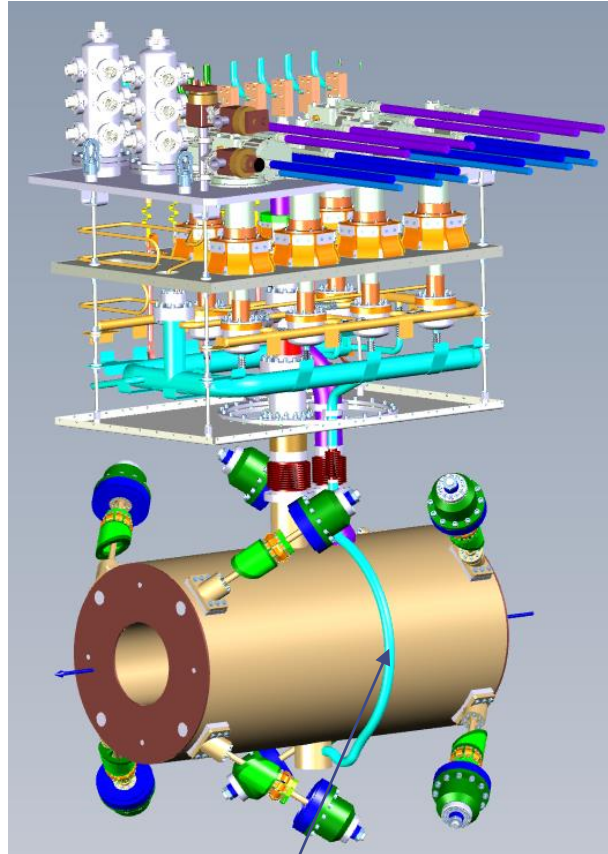
liquid collector



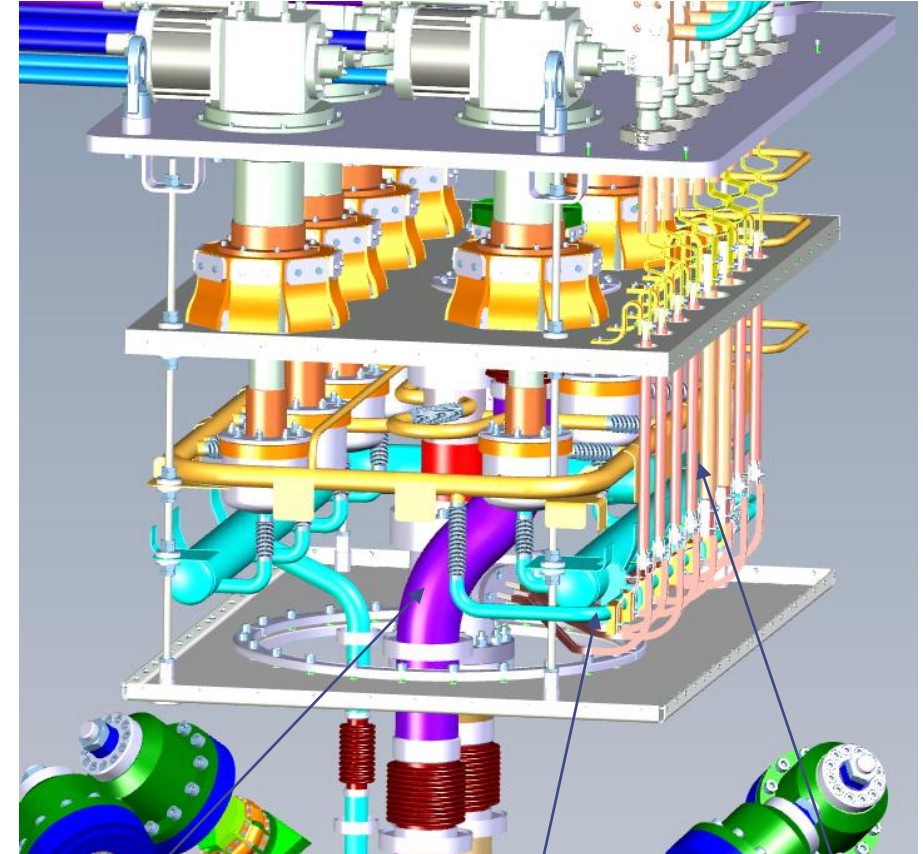
### 3. Cryogenic design (3/3)



Condenser connected to  
Second stage of cryocoolers  
Feed by the gas collector



Liquid helium  
Feeding pipe

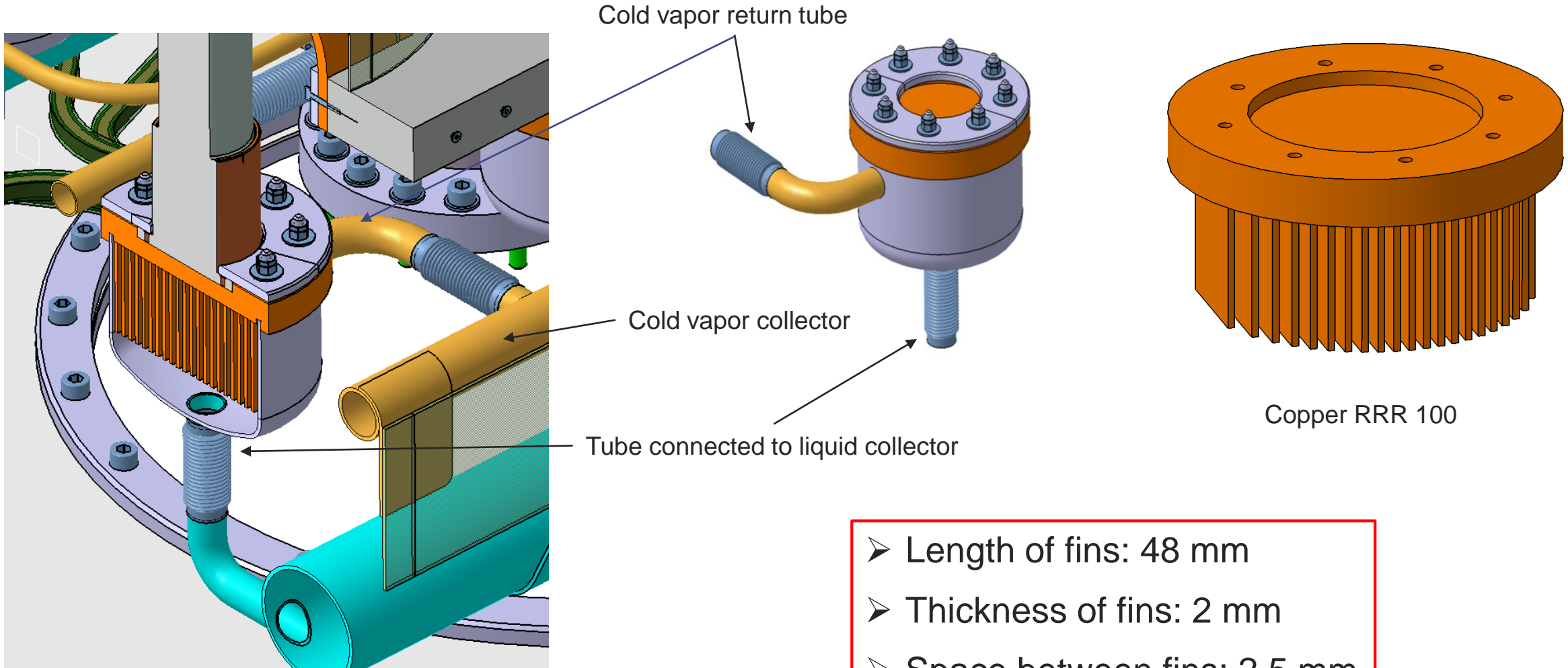


Pressure exhaust  
tube (PED)

Liquid helium tube  
connected to bottom  
of current leads

HTS Current  
leads

# 4. Condenser – same principle as Venus (1/2)





# 4. Condenser – same principle as Venus (2/2)

Heat transfer coefficient for condensation process

Heat transfer in R-5 (condensation process)

$$h_l = 0.943 \left[ \frac{\rho_l (\rho_l - \rho_v) g h_{fg} k_l^3}{L \mu_l \Delta T} \right]^{0.25} = 1322 \text{ W/m}^2\text{K},$$

where  $\rho_l$  = liquid density,  $\rho_v$  = gas density,  $h_{fg}$  = latent heat,  $k_l$  = LHe thermal conductivity,  $L$  = length of fins in HX-2, and  $\mu_l$  = liquid helium viscosity.

**Experimental helium liquefier with a GM cryocooler**

Anup Choudhury; Santosh Sahu

Applied to our condenser, we have for **1** condenser:

- **5 W** as condensation if  $\Delta T = 0.01$  K (very conservative)
- **8.4 W** as condensation if  $\Delta T = 0.02$  K (average from literature)
- Considering **6** condensers with **1.8 W** or **2 W** absorbed at the second stage, we have enough margin for liquefaction (**>>10 W**)

# 5. Current leads

- HTS current leads to limit thermal losses
- Two current leads type:
  - 450 A for the sextupole (1 pair)
  - 210 A for the solenoids (3 pairs)
- One resistive part in brass 70/30 and one HTS part using commercial current leads
- 50 K stage cooled down by conduction
- 4.2 K stage cooled down by conduction through a LHe pipe

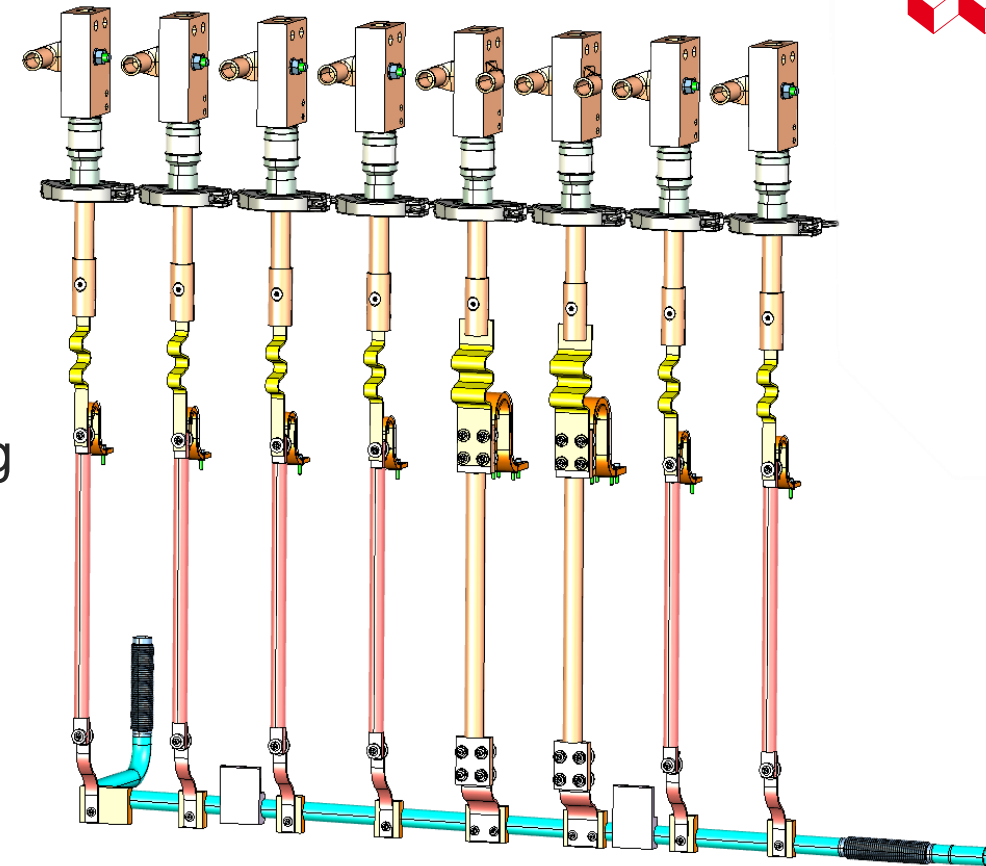
*For brass 70/30*

$$\dot{Q}_{L\ 450\ A} = 22.46\ W\ per\ CL$$

$$\dot{Q}_{L\ 210\ A} = 10.48\ W\ per\ CL$$

$$\dot{Q}_{L\ total} = 107.81\ W$$

$$\dot{Q}_{L\ without\ I} = 12.1 * 2 + 5.7 * 6 = 58\ W$$



*For the HTS part*

$$\dot{Q}_{L\ 450\ A\ HTS110} = 96\ mW\ per\ CL$$

$$\dot{Q}_{L\ 210\ A\ HTS110} = 60\ mW\ per\ CL$$

## 6. Thermal budget at 4 K with 6 cryocoolers (1/2)

Assumption: intercept at 50 K on cryocooler first stage			
	Q (W)	number	Q tot (W)
Dynamic heat load	7	1	7
Tie rods	0.18	8	1.44
Current leads	0.096/0.06	2/6	0.552
PED tube (with below)	0.07	1	0.07
Radiation			0.2
total (W)			<b>~ 9.26 W</b>

- Cryocooler: 1,8 W at 50 Hz or 2 W at 60 Hz
- 6 cryocoolers: 10,8 W or 12 W
- 20% margin -> 11.1 W of cooling power
- Choice to be finalized

## 6. Thermal budget at 4 K with 5 cryocoolers (2/2)

Assumption: intercept at 50 K on cryocooler first stage			
	Q (W)	number	Q tot (W)
Dynamic heat load	7	1	7
Tie rods	0.18	8	1,44
Current leads	0.096/0.06	2/6	0.552
PED tube (with below)	0.07	1	0.07
Radiation			0.2
Failed cryocooler	0.76	1	0.76
total (W)			<b>~ 10 W</b>

- Cryocooler: 1,8 W at 50 Hz or 2 W at 60 Hz
- 5 cryocoolers: 9 W or 10 W
  - 50 Hz ok if  $P_{dynamic} < 6 \text{ W}$
  - 60 Hz ok if  $P_{dynamic} < 7 \text{ W}$

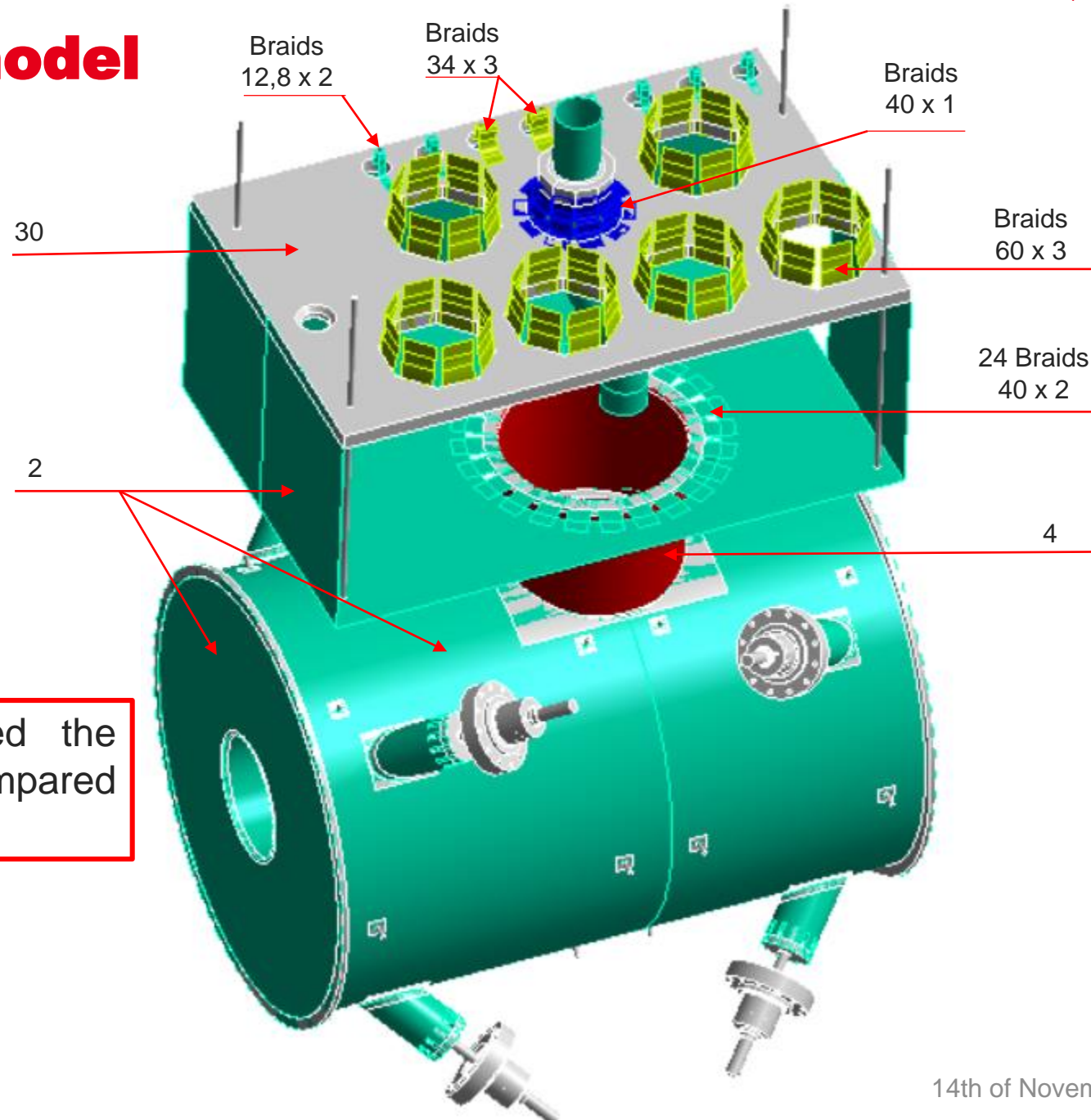


# 7. Thermal shield model

## Geometry






Thickness (mm)

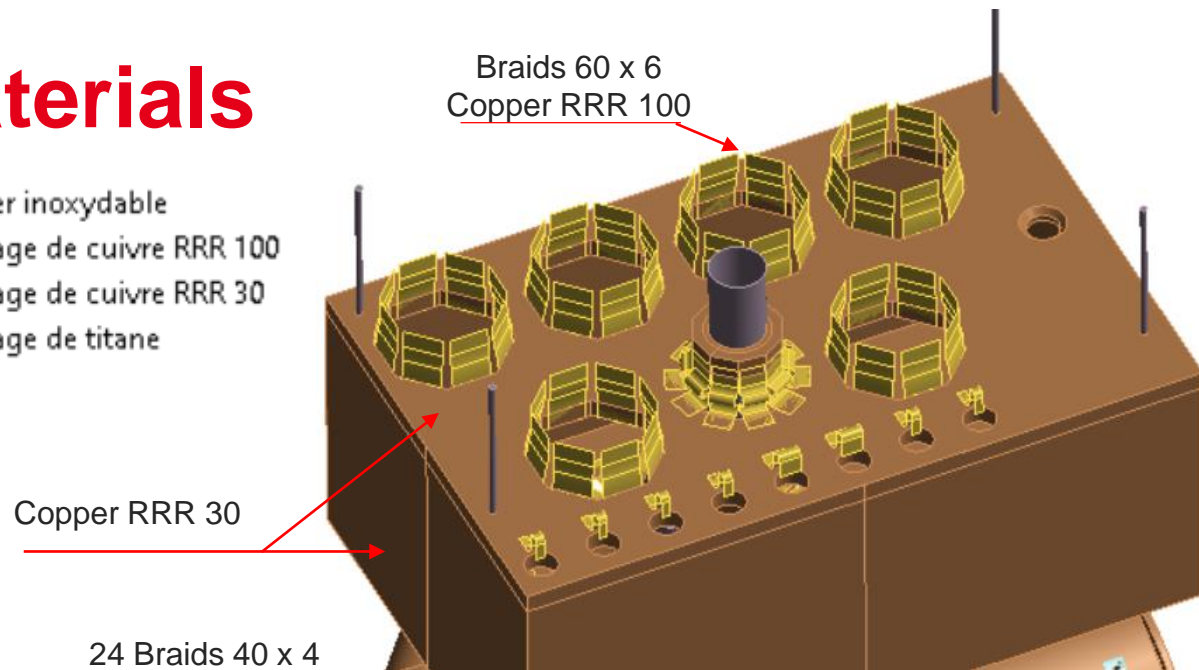
- 4,
- 3,
- 2,
- 1,



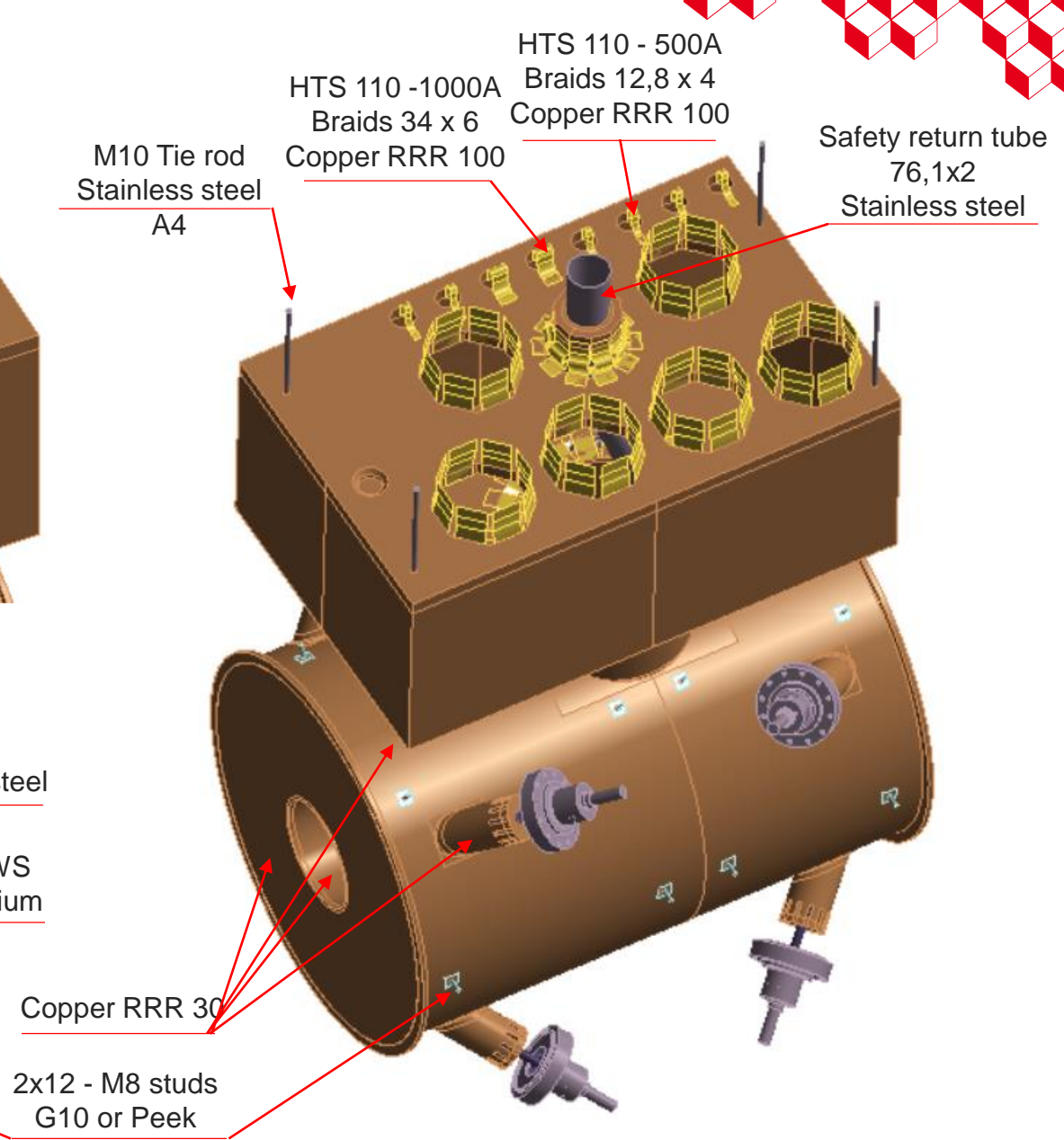
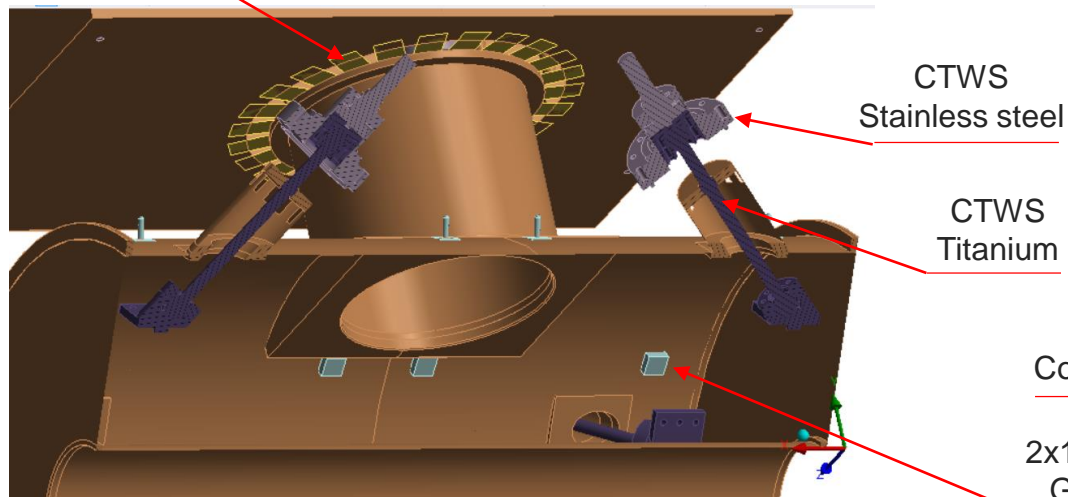
For the calculation, we reduced the thickness of the braids by 50% compared to the design.

# Materials

-  Acier inoxydable
-  Alliage de cuivre RRR 100
-  Alliage de cuivre RRR 30
-  Alliage de titane
-  G10

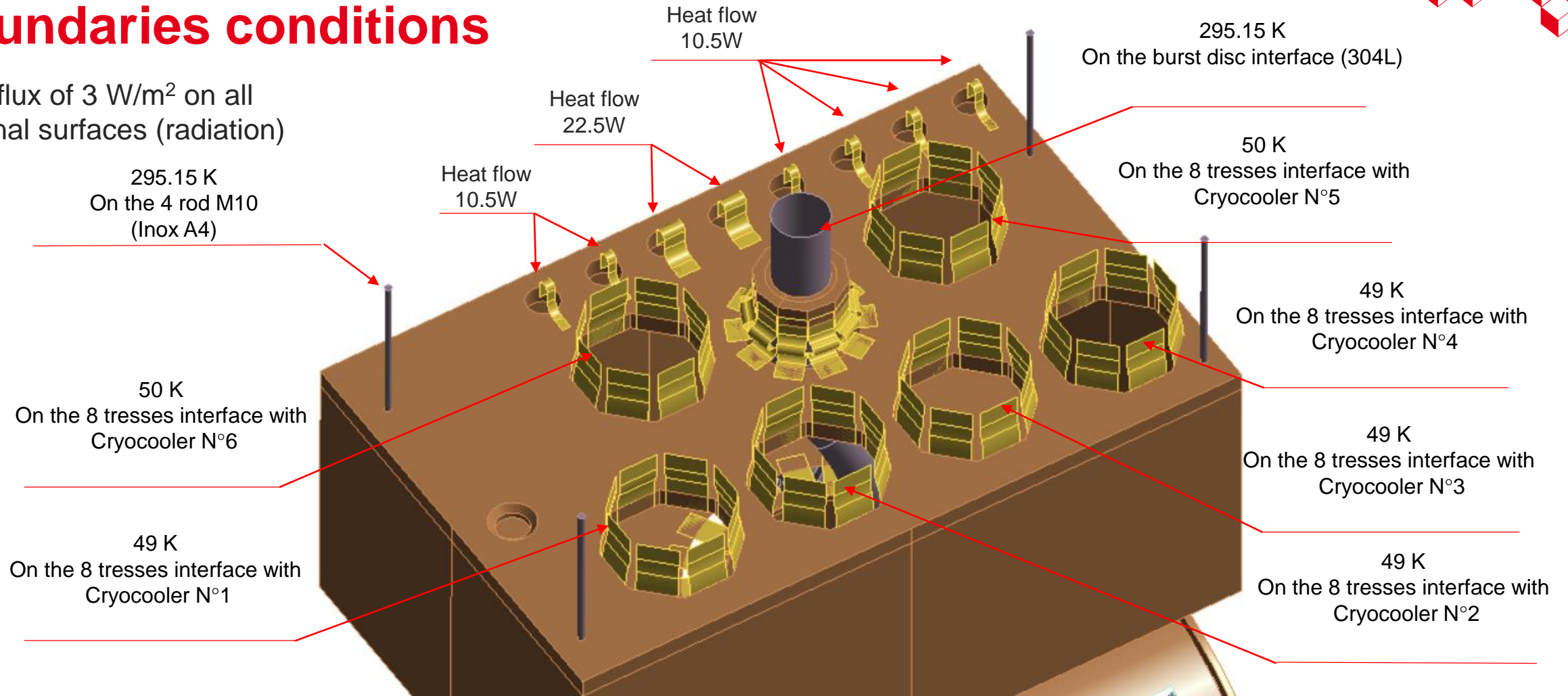


24 Braids 40 x 4  
 Copper RRR 100



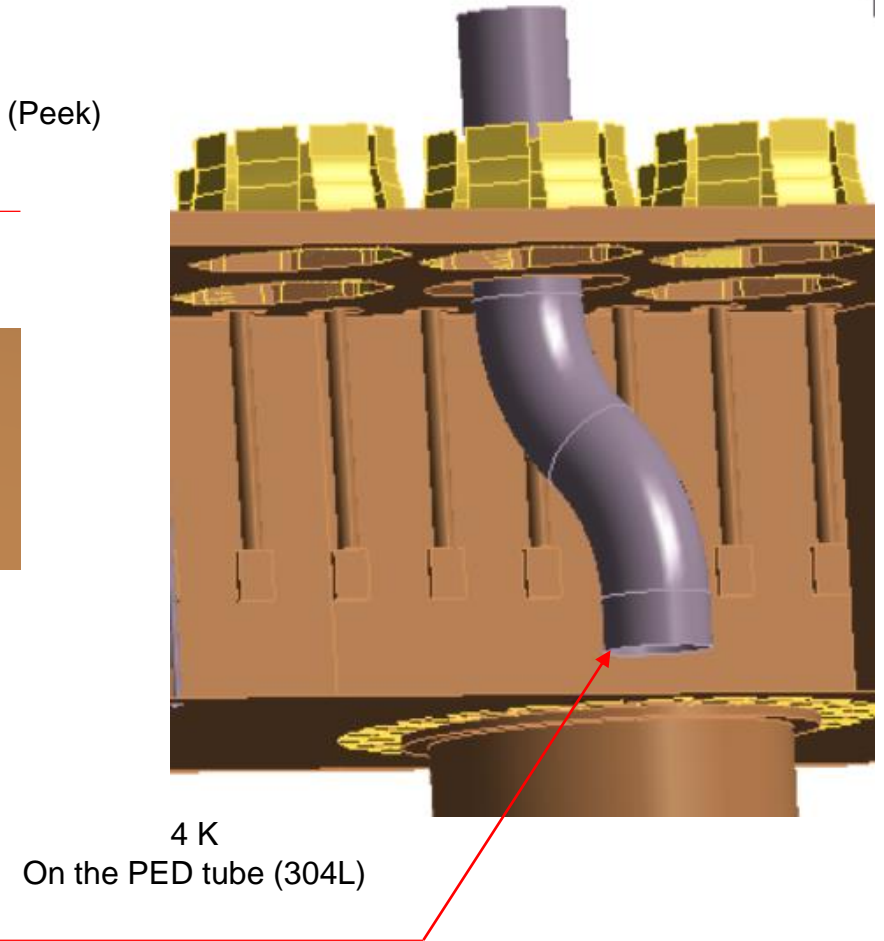
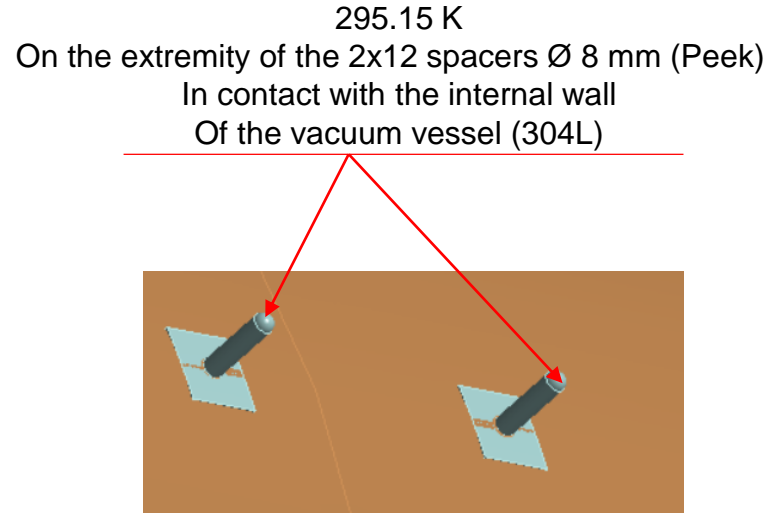
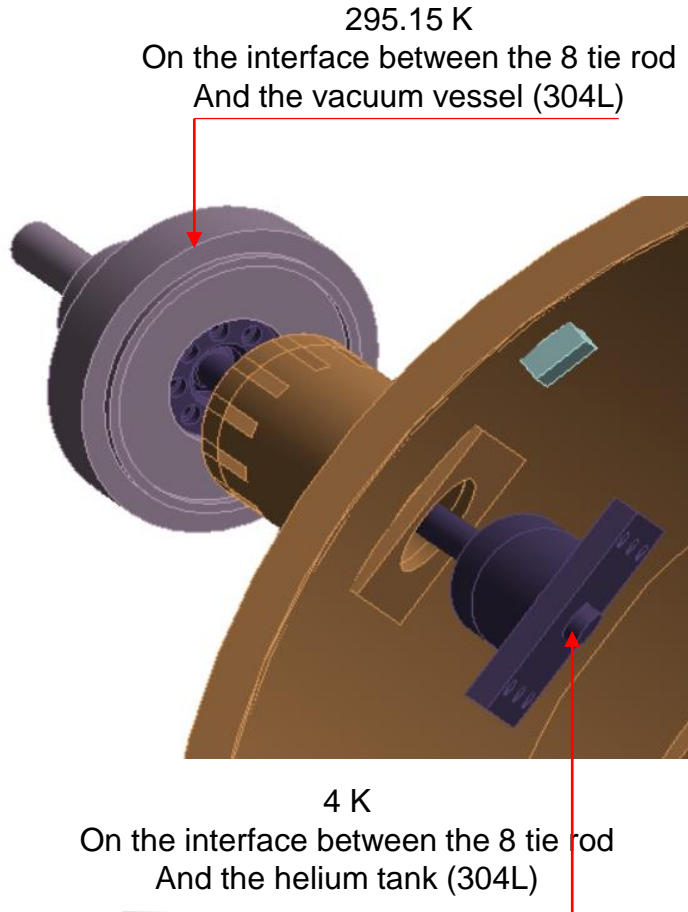
# Boundaries conditions

Heat flux of  $3 \text{ W/m}^2$  on all external surfaces (radiation)





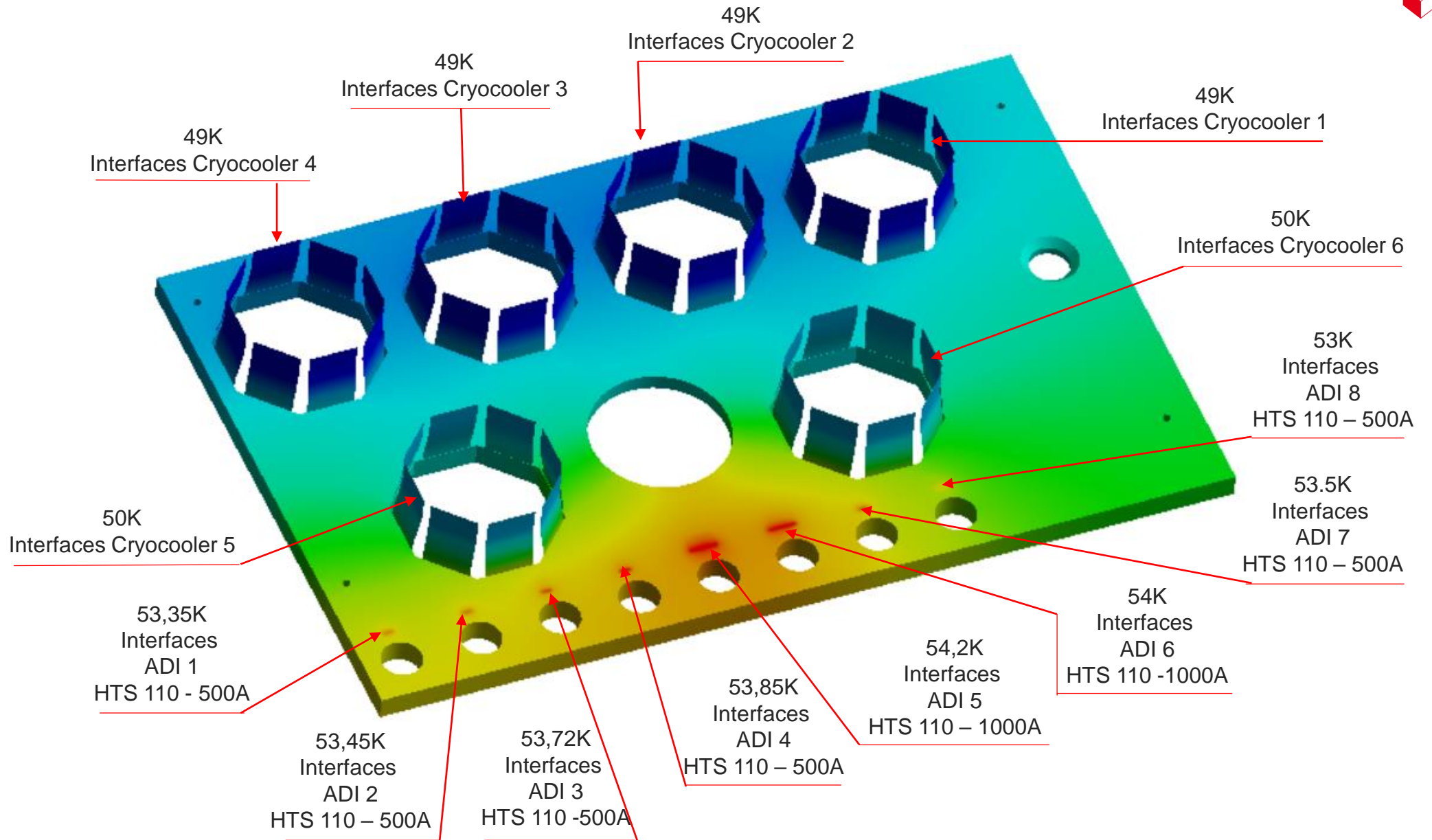
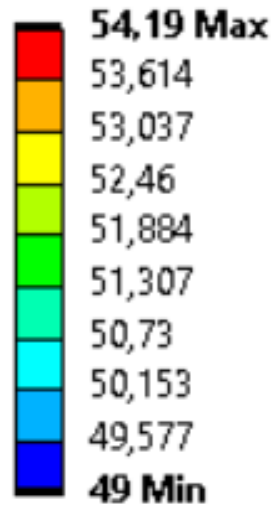
# Boundaries conditions





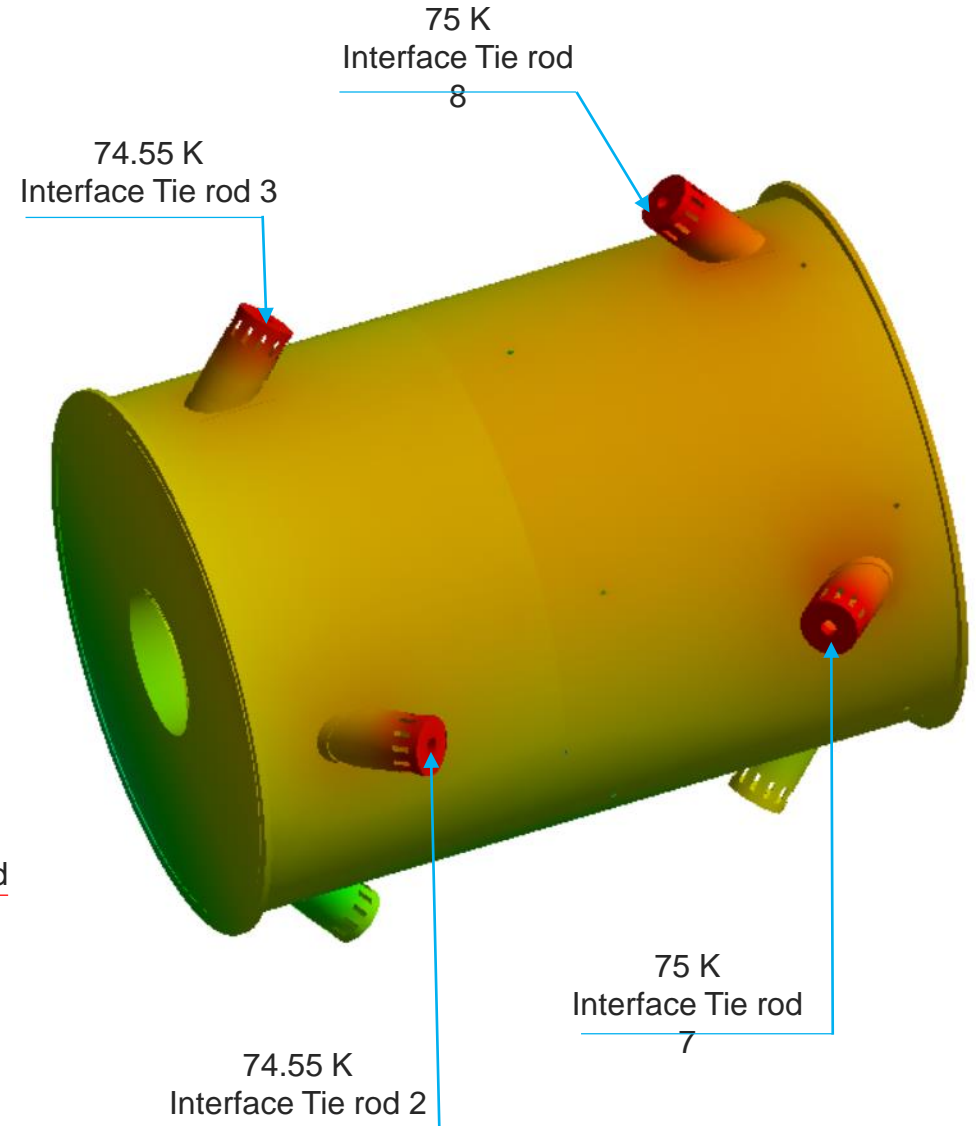
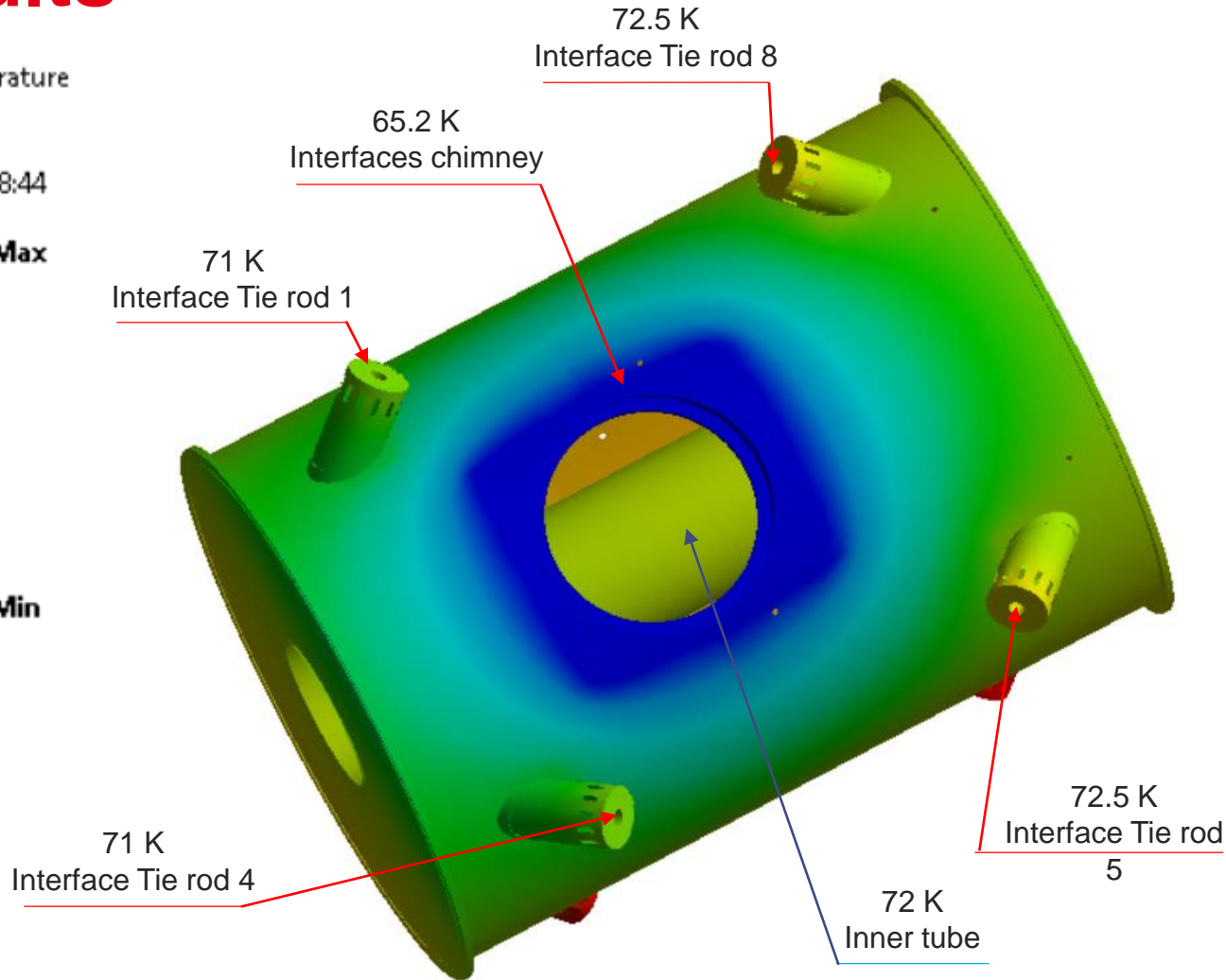
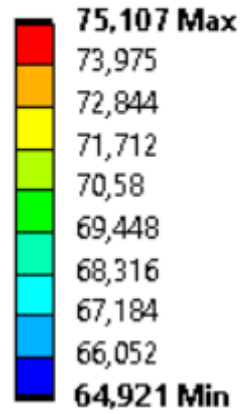
# Results

Type: Température  
Unité: K  
Temps: 1  
29/11/2023 08:21



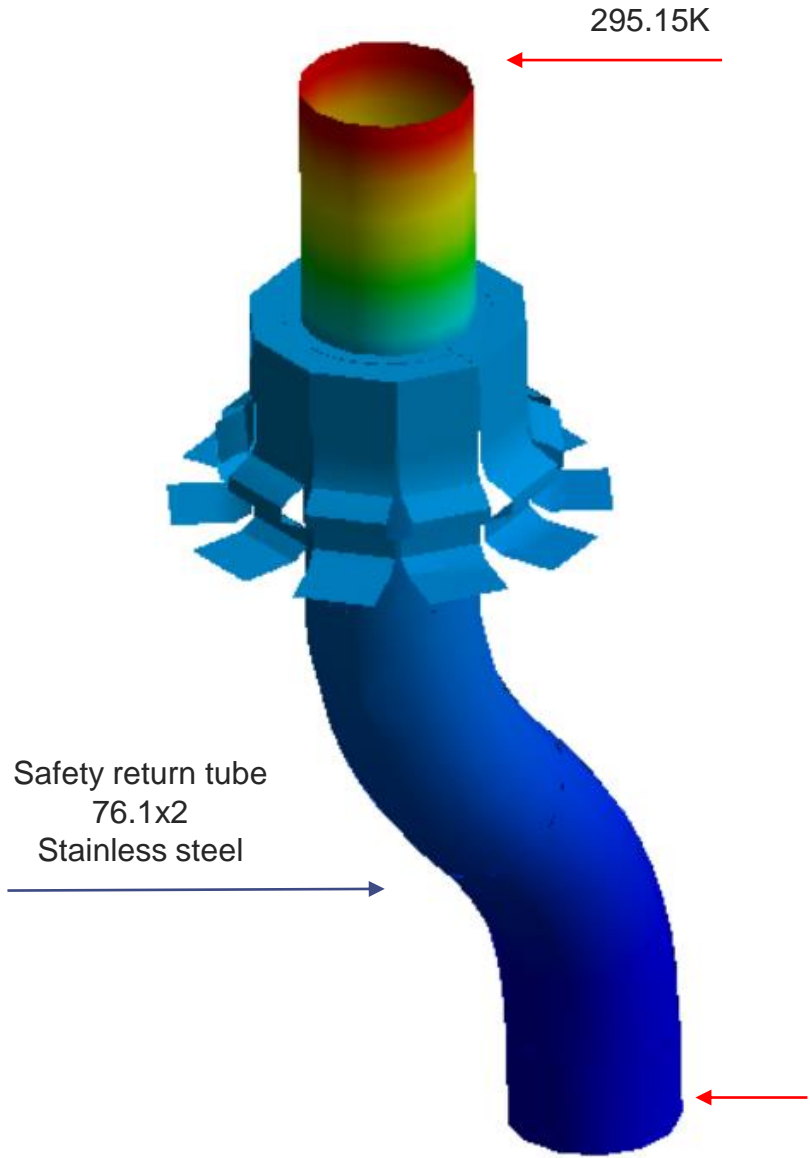
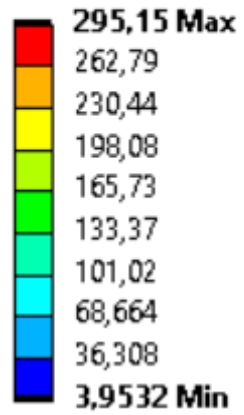
# Results

Type: Température  
Unité: K  
Temps: 1  
29/11/2023 08:44

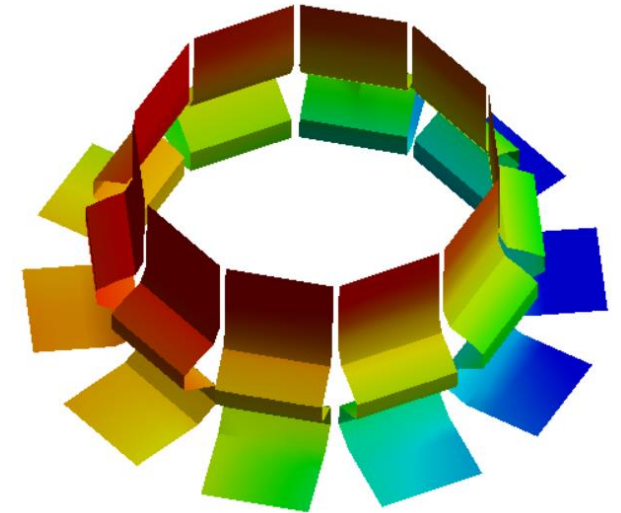
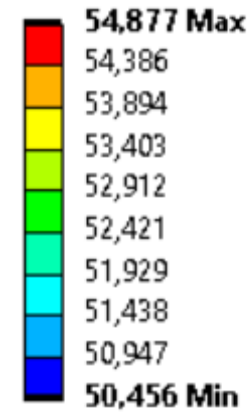


# Results

Type: Température  
Unité: K  
Temps: 1  
29/11/2023 08:51



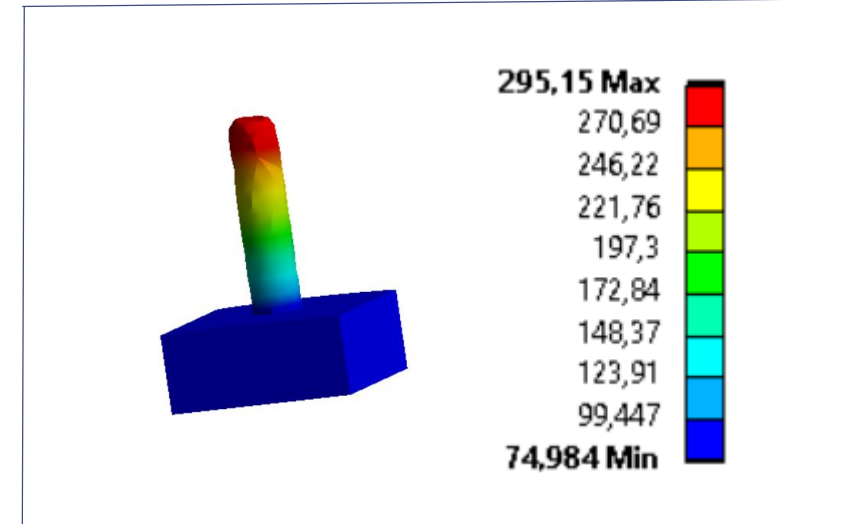
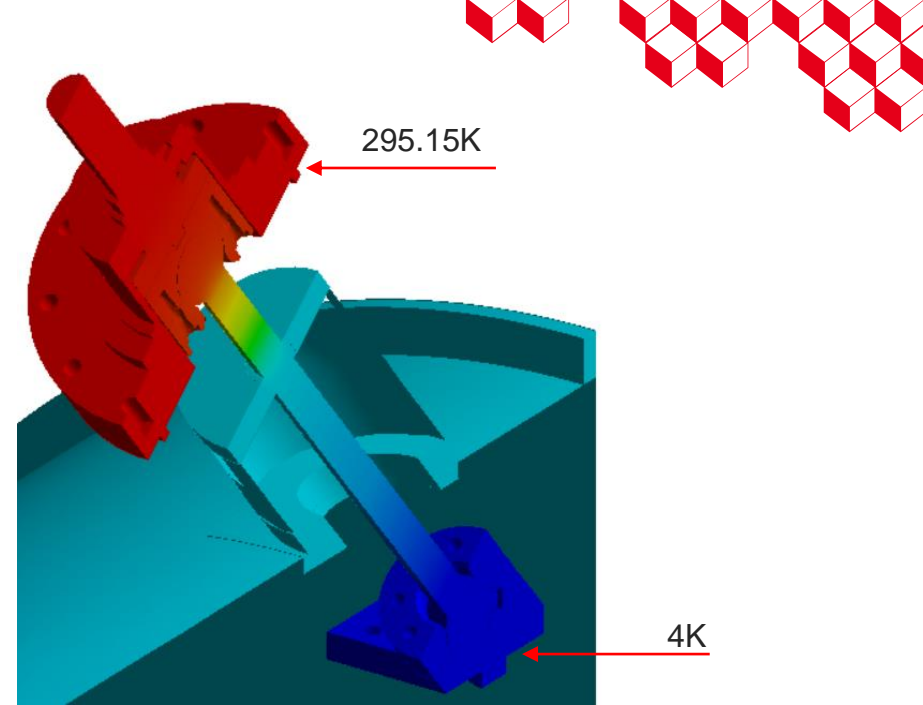
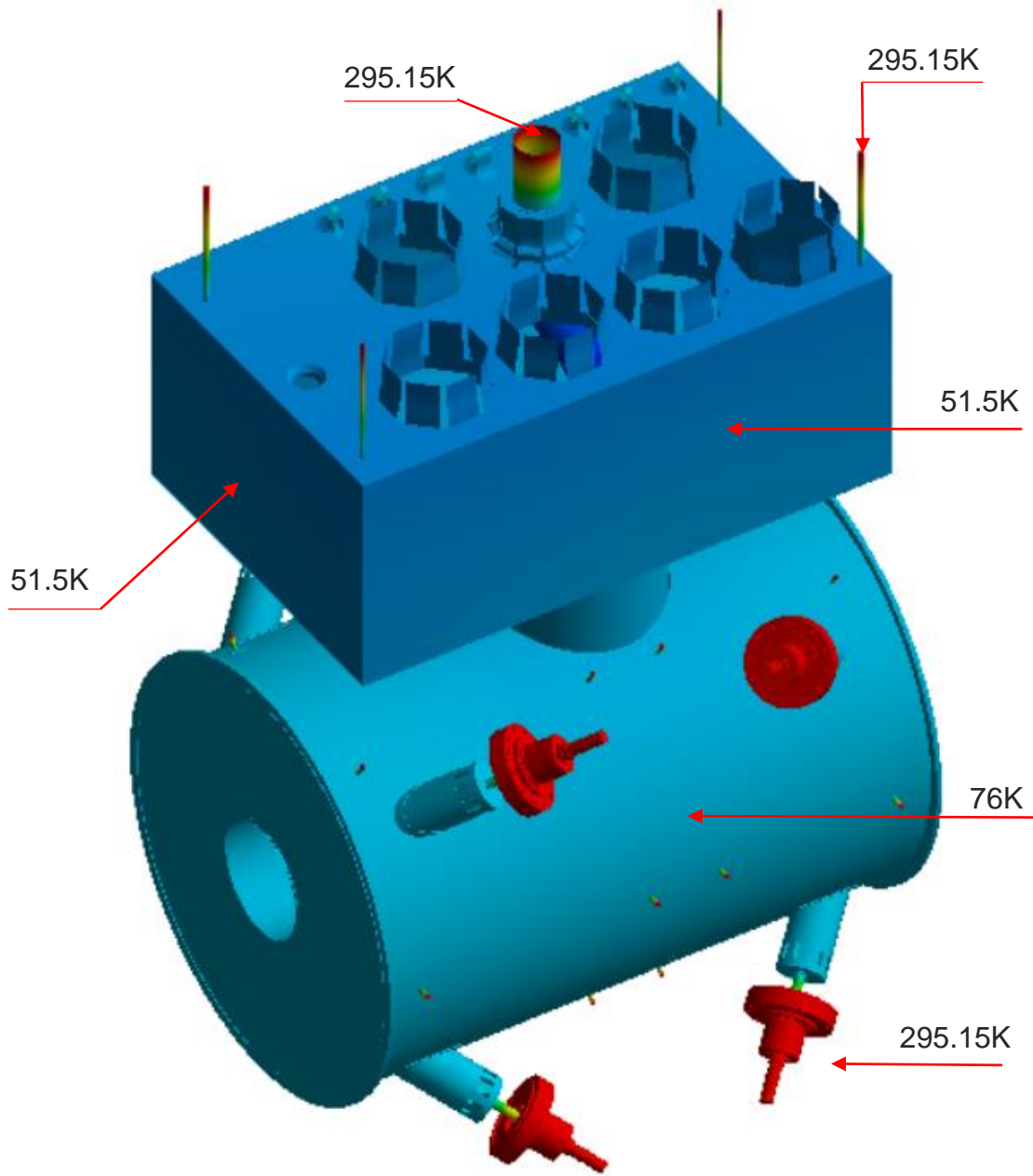
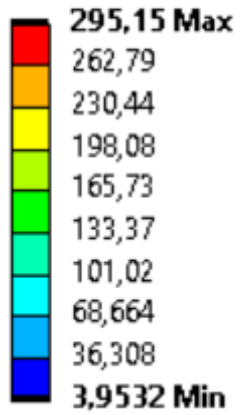
Type: Température  
Unité: K  
Temps: 1  
29/11/2023 08:50



➤ 0.07 W on liquid

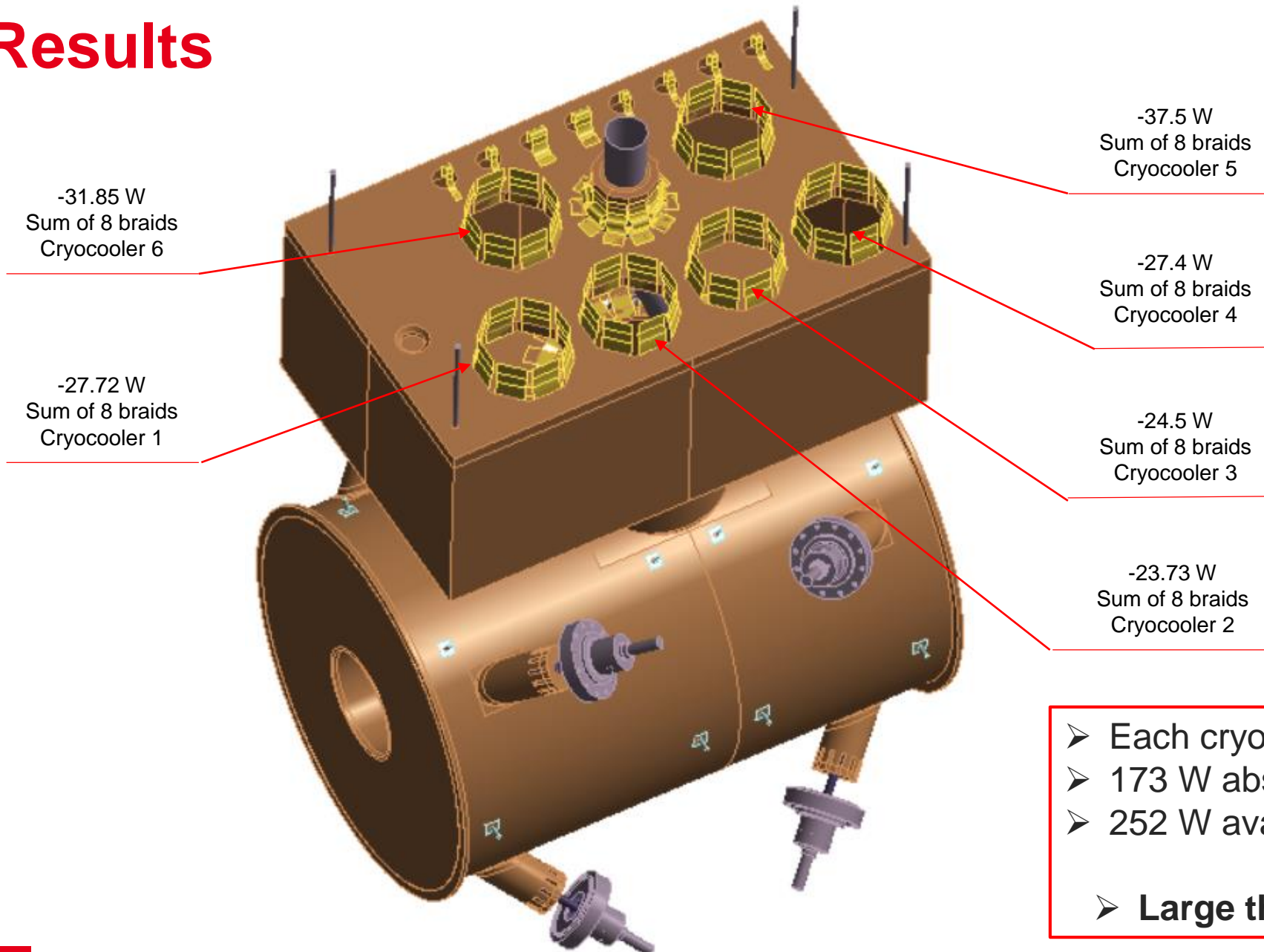
# Results

Type: Température  
Unité: K  
Temps: 1  
29/11/2023 08:52



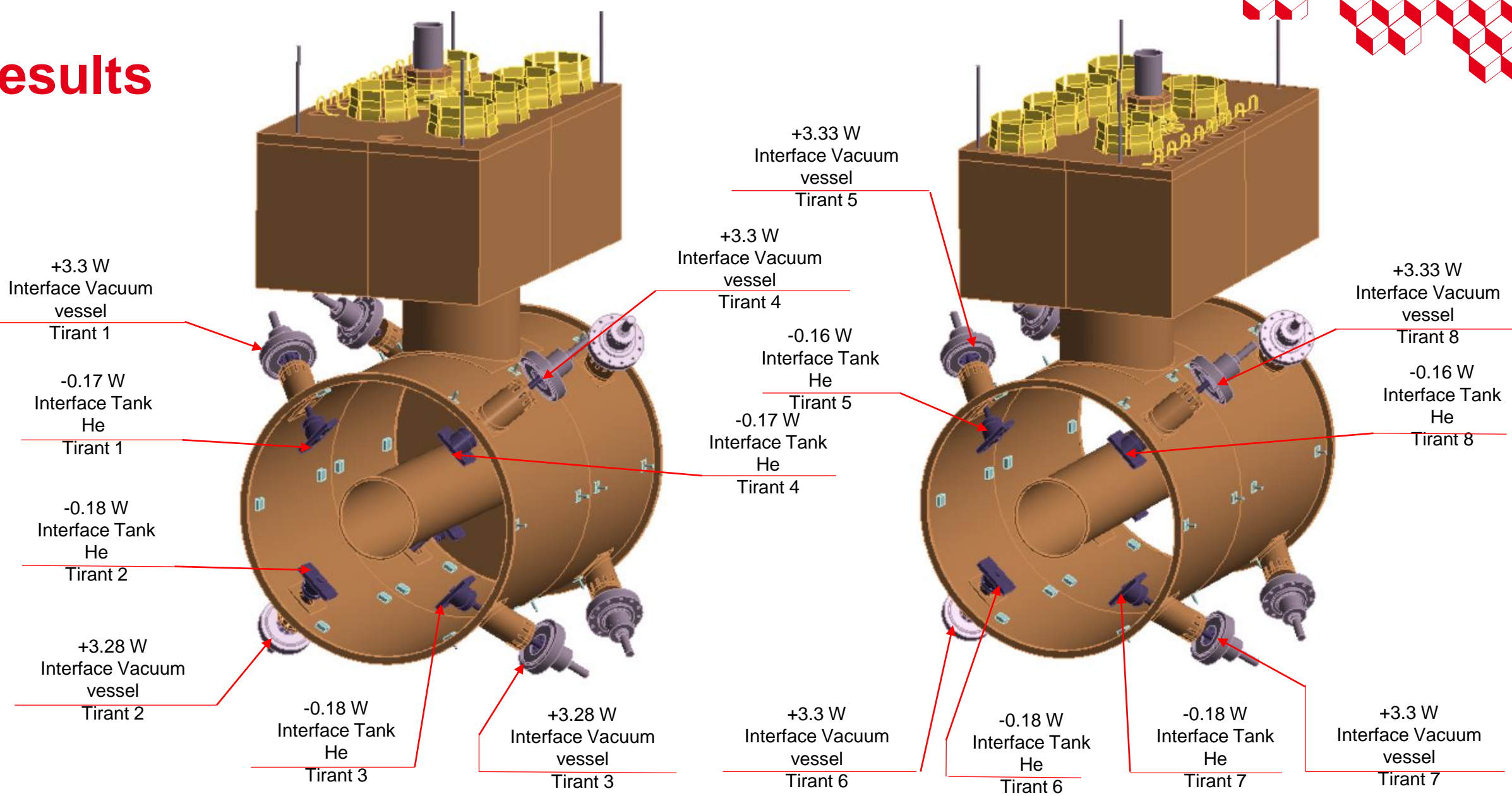


# Results



- Each cryocooler absorbs less than 42 W
  - 173 W absorbed by the 6 cryocoolers
  - 252 W available (42 W per cryocooler)
- Large thermal margin at first stage**

# Results



# 7. Thermal budget at 50 K - summary



Assumption: intercept at 50 K on cryocooler first stage			
	Q (W)	number	Q tot (W)
Current leads	22.5/10.5	2/6	108
Tie rods	3.3	8	26.4
radiation			28
Satellite tie rod	1.1	4	4.4
spacers	0.26	24	6.24
total (W)			<b>~ 173 W</b>

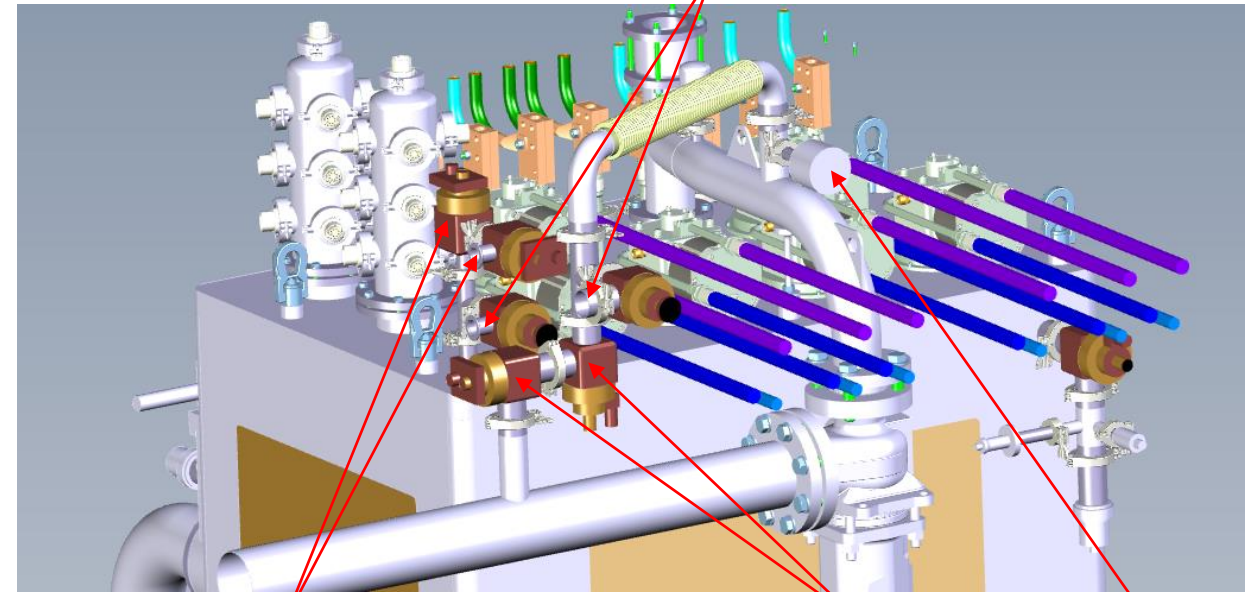
- Cryocooler: 42 W at 50 K
- 6 cryocoolers: 252 W of cooling power available
- Estimated heat load: 173 W
- Margin: 31 %

# 8. Cool down(1/2)

- Rinses:

- pumping by helium gas supply circuit and by PED outlet
- filling with helium gas by helium supply circuit
- 3 rinses considered, need for a mobile primary pumping group (12 m<sup>3</sup>, maximum vacuum at 5.10<sup>-3</sup> mb) (use just for rinsing)

Pumping ports + manual valves



Warm gas helium feeding, feeding and P regulated by valves (1 proportional and 1 open/close)

Pressure regulation valves (1 proportional and 1 open/close)

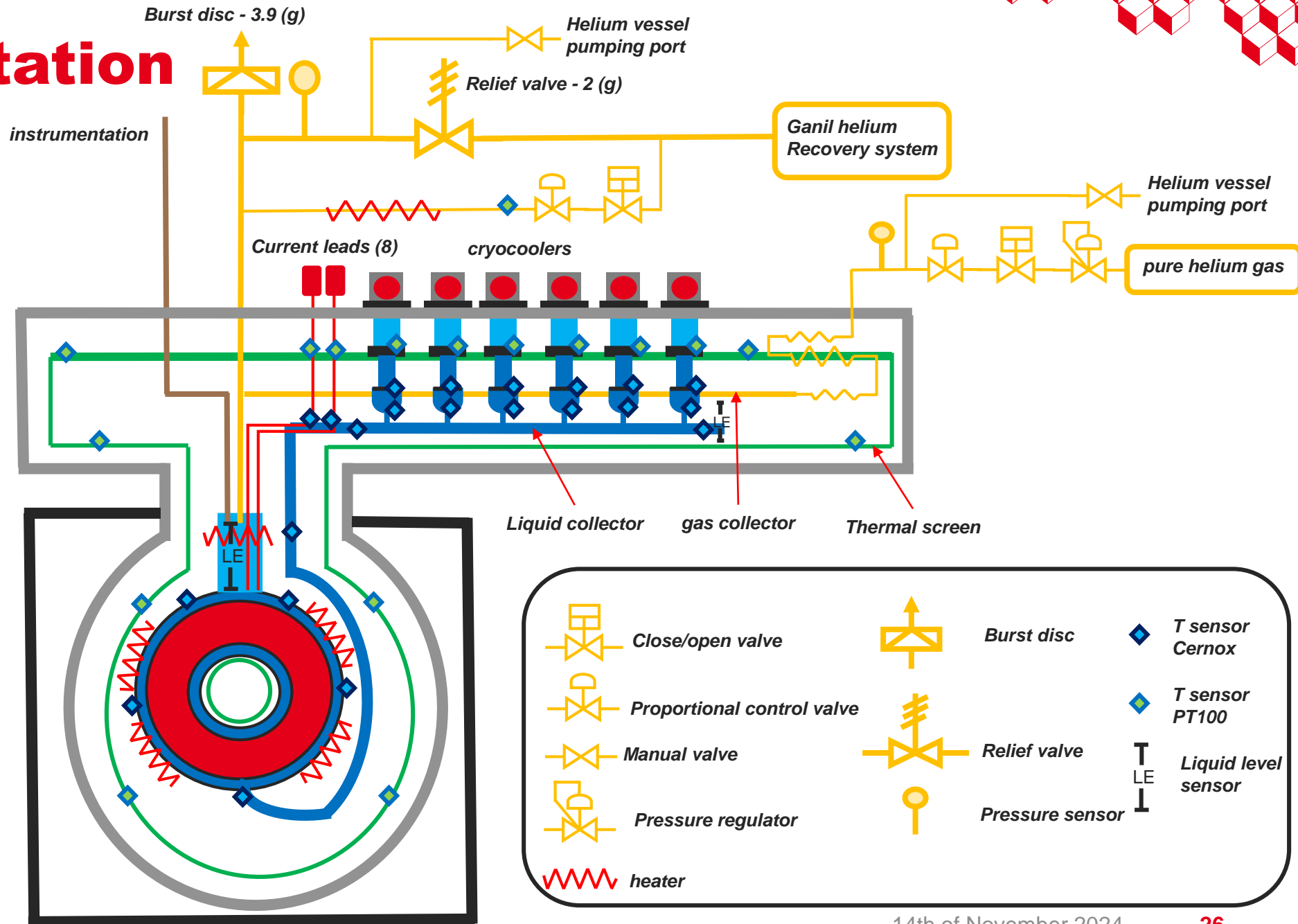
Pressure sensor



## 8. Cool down (2/2)

- **Cool down strategy:**
  - Helium gas supply: 1 open/close valve for sealing and a regulation valve in series ( $C_v = 0.25$ )
  - The control valve will adjust the flow of helium gas to maintain a pressure of 1.2 bar in the helium vessel: 1 regulation system foreseen
  - The gas will cool via the condensers, the pressure will decrease and the difference in density between the cold gas and the hot gas will initiate a convection movement of the helium between the “liquid” collector and the “gas” collector.
  - Cooling time estimated at 5/6 days

# 9. Instrumentation



# 9. Instrumentation - summary

Equipment / sensors	number
Liquid level sensors	4 (only 2 for operation)*
Cernox	22
PT100	22
heaters	2 (+2)* (Lhe level regulation) + 4 (dynamic load)
Pressure sensors	1 (digital) + 1 (with needle)
Proportional valves	2
Open/close valves	2

\*: even if it is redundant heaters or level sensors, it is foreseen to connect the wires up to the leak tight feedthrough if they need to be used. Thus, we can connect them outside and avoid magnet warm up to open the satellite.

# 10. CONCLUSIONS:



- The magnet is cooled by immersion in a liquid helium bath at 1.1 bars and 4.3 K
- The liquid is produced by condensers coupled to the second stage of cryocoolers
- The thermal screen is cooled by coupling with the first stage of cryocoolers
- The calculations and simulations show that we have enough margin with 6 cryocoolers:
  - The maximum total heat load at 4 K is 9.3 W for a cooling power of 10.8 W (12 W also possible)
  - Simulation of thermal screen shows a heat load of 173 W on the first stages for 252 W available
- It is also possible to operate with 5 cryocoolers if one failed
- A system of pipes and valves has been design for the cool down and for the pressure regulation during operation
- The instrumentation has been design to have enough information for the cool down and the operation
- The system is protected from over pressure by a safety valve and a burst disc





**Thank you**  
**Questions?**

