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U.S. DEPARTMENT OF
ENERGY

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SVT Disk Cooling System Manifold - Update

Mechanical and Fluid Dynamic Analysis: Structural Verification and Flow Optimization

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09.23.2025

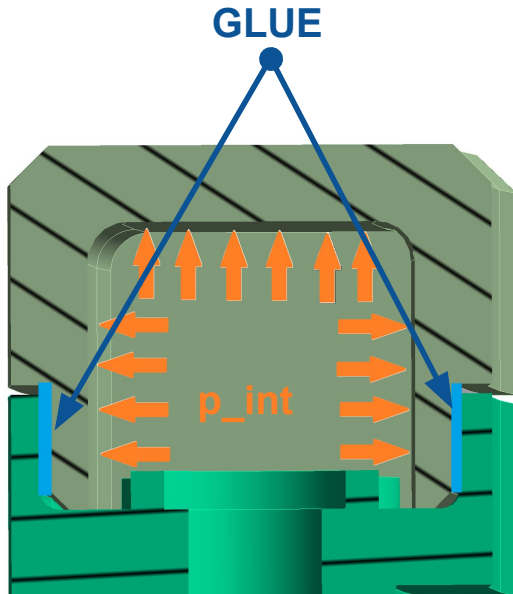
Mechanical Analysis

The goals of this analysis are:

1. Evaluate the effect of material choice on the system's **maximum pressure capacity**;
2. Assess the static strength of the **adhesive joint**.

ADHESIVE JOINT ANALYSIS - Model

Modelling Hypothesis: $E_a = 2 \text{ GPa}$ $\sigma_y = 25 \text{ MPa}$ $f_{os} = 2$



The glue's job is to transfer the load from the upper component to the lower one which is held in place by bolts.

$$T = p_{int} \cdot \frac{A_{up}}{2}$$



$$\tau = \frac{T}{A_{glue}}$$

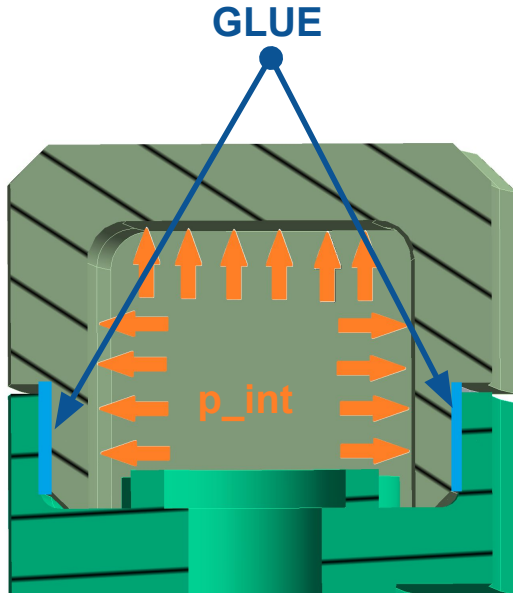
$$F = p_{int} \cdot A_l$$



$$\sigma = \frac{F}{A_{glue}}$$

ADHESIVE JOINT ANALYSIS - Model

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MAXIMUM SHEAR STRESS THEORY

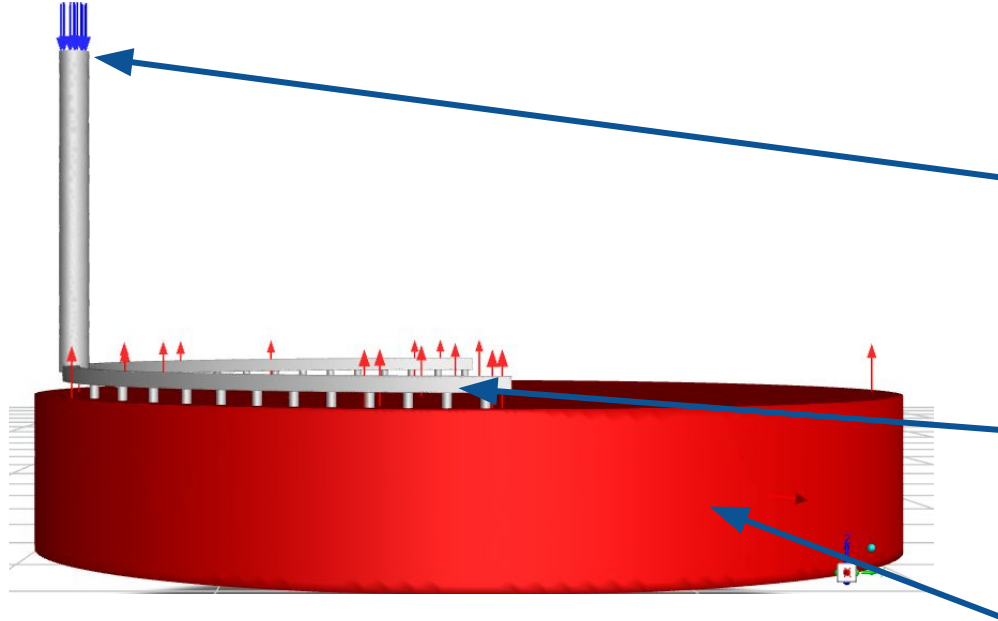
$$p_{int_max} := \frac{\frac{\sigma_y}{f_{os}}}{\sqrt[2]{\left(\frac{A_l}{A_{glue}}\right)^2 + 4 \cdot \left(\frac{\frac{A_{up}}{2}}{A_{glue}}\right)^2}} = 42.446 \text{ bar}$$

Fluid Dynamic Analysis

The goals of this analysis are:

1. To develop a **model** that accurately describes the physical phenomena
2. To **optimize the manifold design** to achieve a uniform mass flow rate through each orifice.
3. **Experimental validation**

CFD MODEL SET UP



PHYSICAL MODEL:

- Fluid: Air as an ideal gas, at 278.15 K
- Turbulence Model: SST
- Analysis type: Steady - state

INLET:

- Type: Mass Flow Inlet
- Value: 0.037 kg/s
- Note: Extended pipe to ensure fully developed flow prior to impingement on the manifold wall.

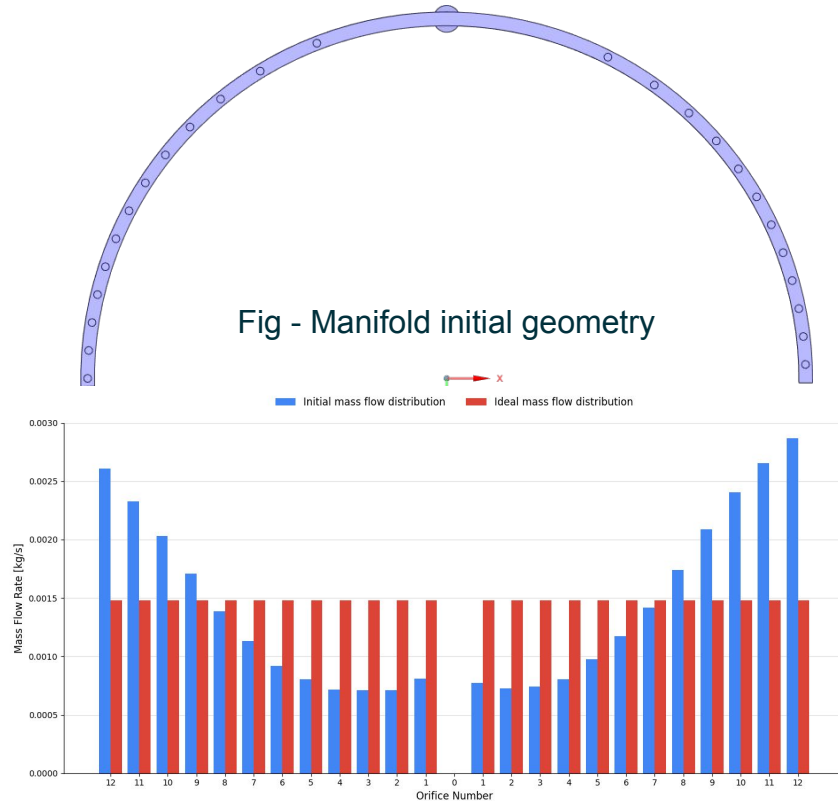
WALL:

- Type: No-slip wall
- Roughness Height: 0.005 mm

OUTLET:

- Type: Pressure Outlet
- Value: 0 (Gauge pressure) - Baseline assumption
- Note: An external plenum (red cylinder) is modeled to avoid imposing artificial back-pressure on the outlets.

OPTIMIZATION



→ Methodology - Parametric Optimization

- ◆ **Design Variables:** The diameters of each orifice (d_i).
- ◆ **Output Response:** The mass flow rate through each individual orifice ($\dot{m}_i$)

→ Target Function - Minimize RMSD

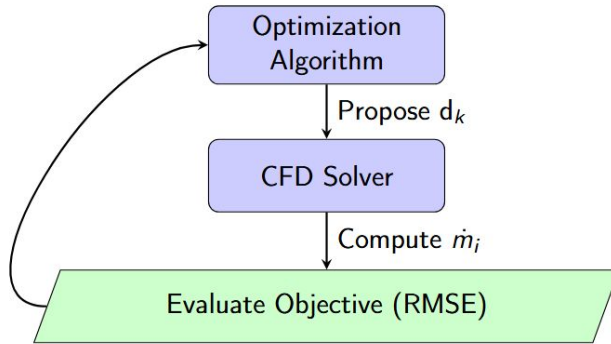
$$\text{RMSD} = \sqrt{\frac{\sum_{i=1}^N (\dot{m}_i - \dot{m}_{\text{target}})^2}{N}}$$

$$\dot{m}_{\text{target}} = \frac{\dot{m}_{\text{tot}}}{\# \text{orifices}} = 0.00148 \frac{\text{kg}}{\text{s}}$$

OPTIMIZATION - Method [2]

Problem: Very high computational cost of CFD simulation

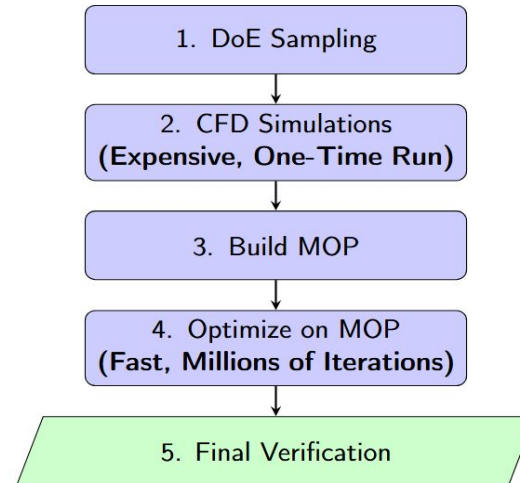
Direct optimization process



X Very slow

X High Risk of Local minimum

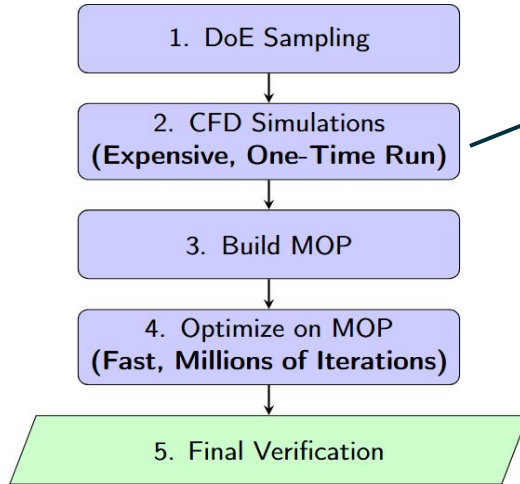
Metamodel-based Optimization



OPTIMIZATION - Method

Problem: Very high computational cost of CFD simulation

Metamodel-based Optimization [3]



Train a metamodel using CFD simulations to achieve a high **Coefficient of Prediction**.

X Complex geometry needs many points to create a MOP with high CoP

Attempt 1: model without plenum:

- 50 Samples
- CoP = 0.9
- 10000 iteration

OPTIMIZATION - Results 1

Non-uniform mass flow distribution

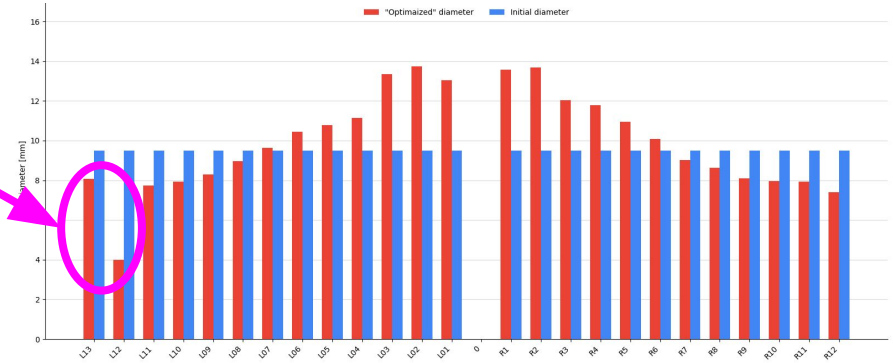
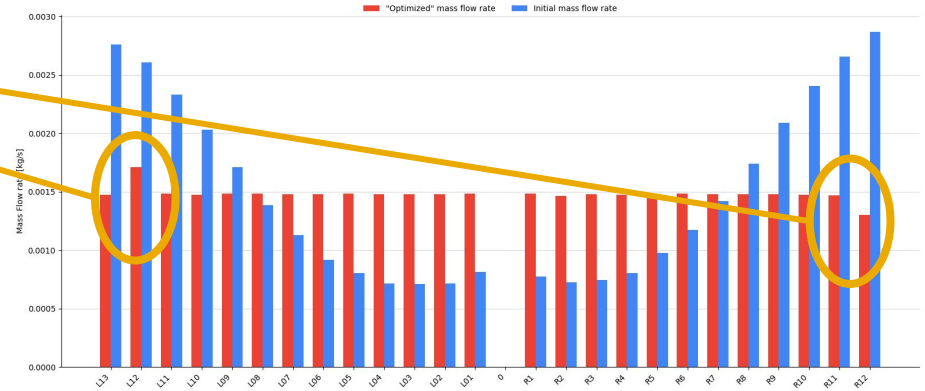


Caused by the non-uniformity in the diameter trend

The simple model generates numerical issue

Hp: Without Plenum p_{atm} is applied directly at each orifice -> like a pump

Mass flow rate

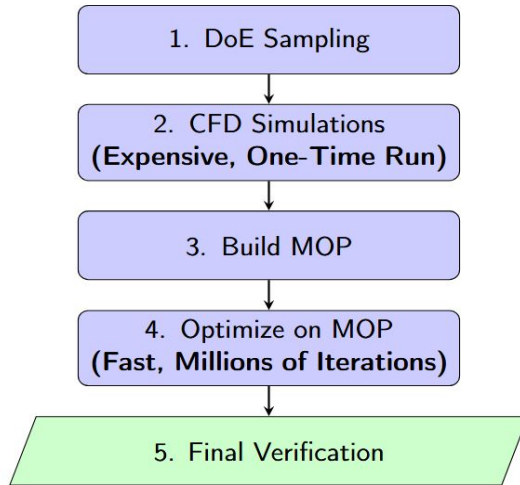


Diameters

OPTIMIZATION - Current status

Problem: Very high computational cost of CFD simulation

Metamodel-based Optimization



Attempt 2: model with plenum:

- 100 Samples
- CoP = 0.2

CoP is too low - a larger sample size is required

Attempt 3: model with plenum:

- 300 Samples
- CoP = ? *currently running*

Increasing the sample size is time-consuming

SUMMARY

- Assessed the static strength of the **adhesive joint**.
- Evaluated **different optimization approaches**.
- Defined and performed a **sensitivity analysis** and the **subsequent optimization**.

NEXT STEPS

- **Analyze** the final optimization results.
- **Conduct experiments** to validate the simulation results