



An electric-circuit model of inter-tape contact resistance and current sharing for REBCO cable

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Main driving questions

- What is an appropriate model to provide the insight on the impact of contact resistance in REBCO cables?
- What is the optimal contact resistance R_c for REBCO cables to address the needs between current sharing and to suppress excessive Eddy currents?
 - Would current sharing benefit the cable performance in the presence of a localized defect?
- What is the impact of having I_c and n-value variations on the performance of different REBCO cable configurations?





Outline

- 1) Introduction of the n-Stacked-Tape Cable model
- 2) Validation of the model
- 3) Applications

- Simulations and measurements of a localized defect and current sharing in stacked-tape cable

- Monte Carlo simulations of *I_c* and n value variations in n-Stacked-Tape Cable

4) Conclusions and next steps





Stacked-tape case





We developed a simple electric-circuit model based on Ngspice to study the impact of contact resistance on stackedtape cable



*Impact of magnetic field on the I_c not considered





Validation of the model





We reproduce the published results as a first validation to the model



Takayasu *et al.,* IEEE TAS 2016 DOI 10.1109/TASC.2010.2094176







Our model reproduced the current distribution



• Tapes with lower termination resistance carry a higher amount of current until the cable critical current is reached





Simulations and measurements of a localized defect in stacked-tape cable





We studied the impact of a localized defect in the 2-tape cable with two cases: tapes isolated and soldered







We tested both cases with SuperPower 4 mm wide tapes at 77 K, self-field

- Three voltage sections, each 2 cm long
- A defect in the center section of tape 2
- Data from the measured I_c/n at self-field were used in calculations

Section	I _c (A)	n
V1	132.3	30.5
V2	89.4	24.2
V3	133.1	31.0
V4	133.1	28.9
V5	130.7	30.7
V6	131.8	29.7



Current leads



Defect





We performed two types of $\rm I_{\rm c}$ tests on the 2-stack of tapes: insulation and solder between tapes.

Tapes isolated with Kapton tape



Tapes soldered with $Pb_{40}Sn_{60}$ solder



 $R_c = 1000 \Omega$ used for the insulated case

 $R_c = 46 n\Omega^*$ used for the soldered case

*Solder conductivity 0.27x10⁸ S/m at 77 K Yeekin Tsui *et al* 2016, *SST* **29** 075005



Simulations qualitatively agree with measurements: insulated case





09/18/2019



Simulations qualitatively agree with measurements: soldered case

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The voltage rise observed for the soldered case was not due to the potential degradation in the sections during soldering

- We un-soldered the tapes and measured I_c and n-value for each tape separately to verify if degradation of the tapes has occurred
- I_c degradation < 3%. Negligible change on n value

	HTS	I _c (A)		n	
	section	Before	After	Before	After
	V1	132.3	*	30.5	*
Defect section	V2	89.4	86.7	24.2	24.4
	V3	133.1	*	31.0	*
	V4	133.1	130.4	28.9	28.8
	V5	130.7	129.9	30.7	29.9
	V6	131.8	129.2	29.7	28.3

* Values that could not be measured after





With the validated model, we can now shed light on how the contact resistance affect the current bypassing the defect





Reminder on the model



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Low contact resistance allows current to bypass the damaged section when approaching its critical current.







In the case of high contact resistance current sharing is determine by the terminal resistances



V2

V3

GND

I_{cable}

 R_t

V1

 R_t

♡

GND

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Low contact resistance reduces the heat generation



• We need to reduce contact resistance to reduce the temperature rise during transition





Cable I_c is increased 2% when the contact resistance is 10 $n\Omega$



• Rc = 10 nΩ

- $I_c = 150.1 \text{ A}, n = 32.5, \text{ Fit-error} = 2.299 \times 10^{-7} \text{ V}$
- Rc = 1000 Ω
 - I_c = 148.1 A, n = 22.9, Fit-error = 2.40016x10⁻⁵ V





We can estimate the threshold value for the R_c to achieve good contact



Optimal R_c depends on termination resistance.

Rt	Good contact (Ω)
25 μΩ	≤ 10 µ
250 nΩ	≤ 100 n
2.5 nΩ	≤ 1 n

tape 1= 100 A; tape 2=50 A. n = 30





Monte Carlo simulations of *I*_c and *n*-value variations in the stacked-tape cable





We performed Monte Carlo simulations to study the impact variations in I_c and n-value on the cable performance

• We used the power law to model the voltage in the superconducting tapes

$$V_{b_{i}} = E_{c} * L \left(\frac{I}{I_{c}}\right)^{n}$$

$$V_{terminal} = V_{b_i} + \frac{R_i}{n} * I_{cable}$$

- $E_c = 100 \ \mu V/m$
- L = 1 m
- R_i = 500 nΩ



*Pothavajhala *et al.,* IEEE TAS 2015, 2371923 *I_c* and n-value variations along the tape length 24



We calculated the terminal V(I) transitions with different standard deviations of the normal distribution of I_c and n-value with population size of 500







Tapes with different Ic affect the cable n value more than the cable Ic



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Tapes with different n values affect less cable Ic and nvalue than tapes with different Ic values







Conclusions and next steps

- We developed a simple circuit model to help understand the impact of contact resistance and current sharing for REBCO cables
 - The model reproduces the published results on stacked-tape cable
 - Qualitative agreement with measurements in 2-tape stack cable soldered and with insulation
- As expected, low contact resistance allows current to bypass defects and to reduce the power generation during the transition. The value for the R_c to achieve good contact depends on the termination resistance.
- Cable I_c and n-value are more affected by the variation of I_c in the tapes than the variation of n-value. Cable Ic reduces by less than 5% when $\sigma(Ic) < 30\%$.

We are now working to

- Include inductances in the cable model to study the non steady-state cases
- Develop an model for CORC wire to understand the impact of contact resistance



Additional slides

09/18/2019





We can understand the voltage and current distribution in a 2-tape cable

