

# Cryogenic electronics for superconducting magnet instrumentation

**M. Marchevsky**

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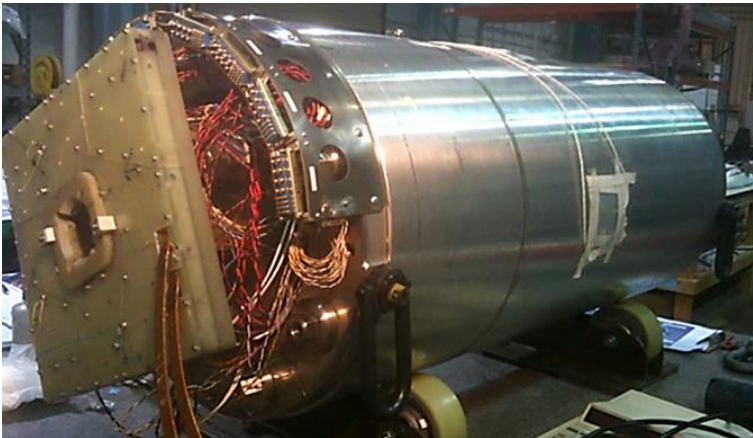
*Lawrence Berkeley National Laboratory*

Work conducted for the US Magnet Development Program and Fusion programs funded by the DOE under  
Contract No. DE-AC02-05CH11231

Temperature  
Strain

**Performance  
monitoring**

Field quality



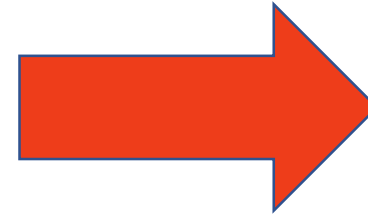
Coil voltage

Acoustic emission

**Quench detection  
and localization**

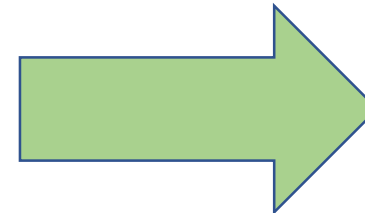
Magnetic field  
disturbances

Fast datastream ( $\sim 1\text{Ms/s /ch}$ )



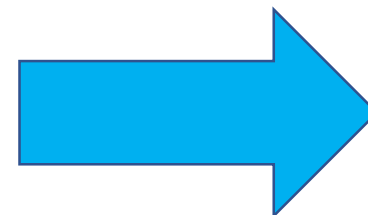
(AE, field disturbances)

Medium datastream ( $\sim 10\text{-}100\text{ kS/s /ch}$ )



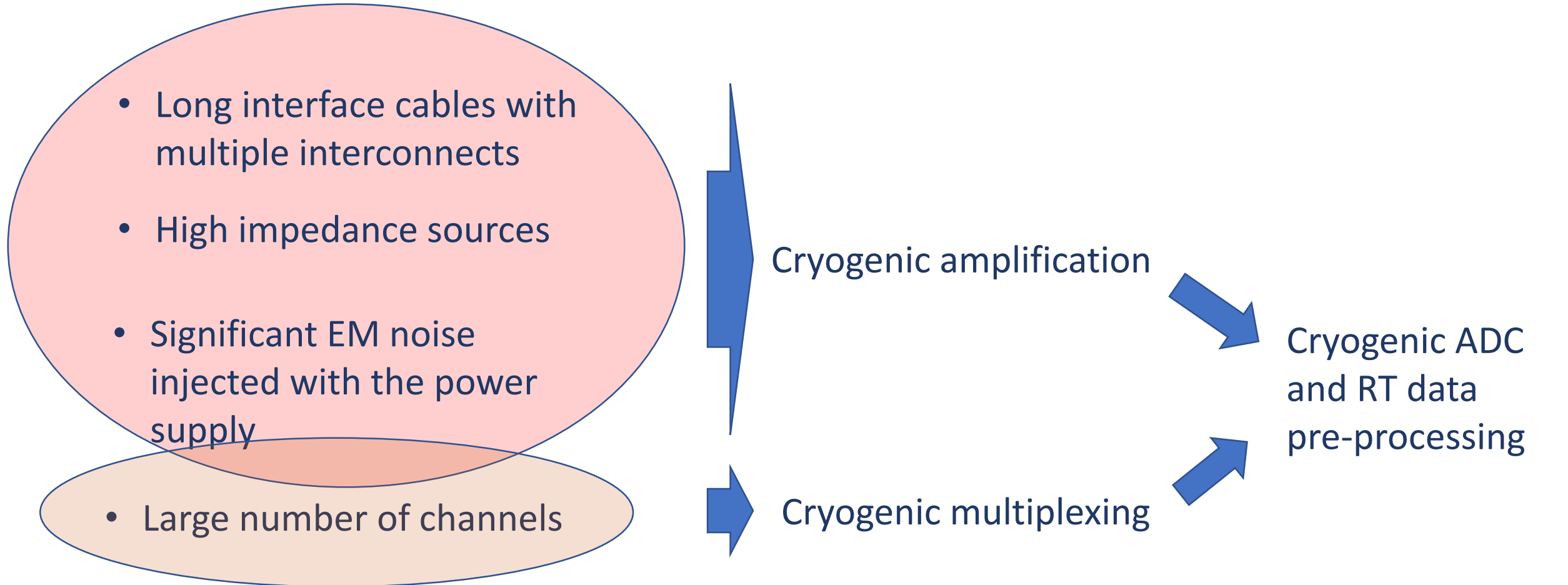
(Voltage, field  
quality probes)

Slow datastream ( $\sim 1 - 1000\text{ s/s /ch}$ )



(Strain, temperature)

# Benefits of using cryo-electronics for magnet instrumentation

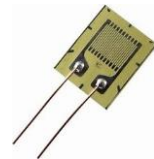
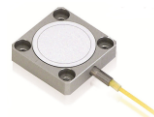
- 
- Long interface cables with multiple interconnects
  - High impedance sources
  - Significant EM noise injected with the power supply
- Large number of channels

Cryogenic amplification

Cryogenic multiplexing

Cryogenic ADC  
and RT data  
pre-processing

## Sensors

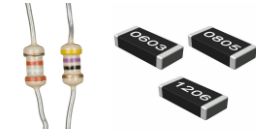
- Wire loops (quench antennas) 
- Resistive strain gauges 
- Capacitive sensors
- (affected by the cryogenic liquid) 

Temperature is not a significant factor

- Hall effect sensors (GaAs) 
- Acoustic emission sensors made with piezoelectric ceramics 

Sensitivity decreases,  
quality factor increases

## Passive components

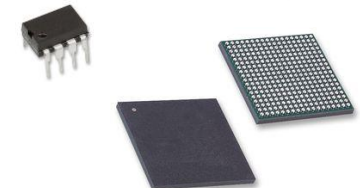
- Resistors (metal film) 
- Capacitors (XOR, tantalum) 
- Diodes 

Temperature is not a significant factor

Capacitance decreases

Forward voltage drop increases

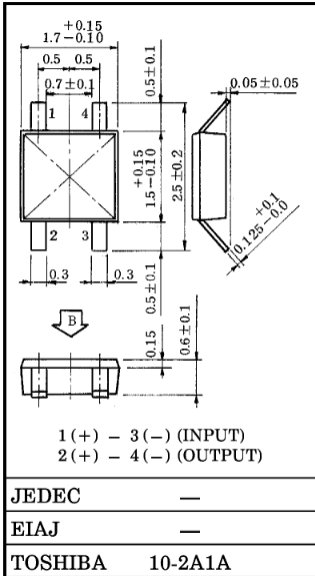
## Active components

- MOSFETs and MOSFET-based ICs 
- Op-amps (CMOS, SiGe) 
- Digital electronics, FPGA 

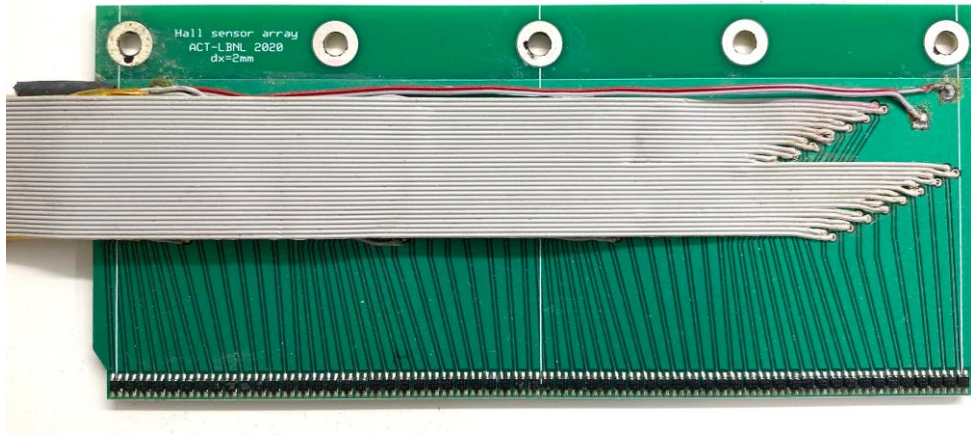
Many work cryogenically, but require some adjustment of operational conditions

THS121

Unit in mm



Weight : 0.0047g

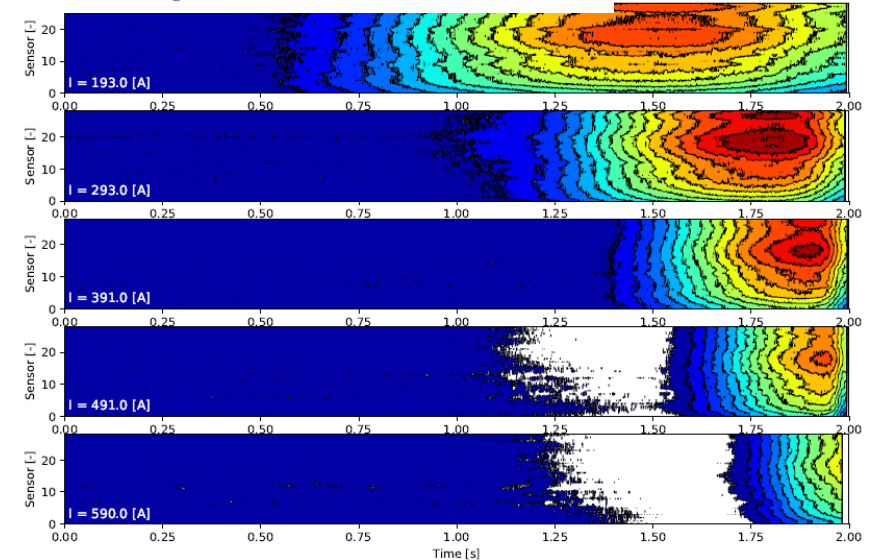
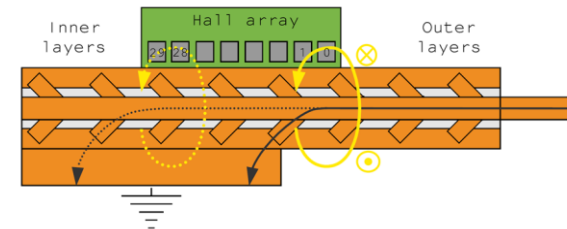


A linear array of 60 Hall sensors for quench detection / quench propagation studies

ELECTRICAL CHARACTERISTICS ( $T_a = 25^\circ\text{C}$ )

| CHARACTERISTIC                   | SYMBOL         | TEST CONDITION                                                                                 | MIN. | TYP. | MAX.     | UNIT                        |
|----------------------------------|----------------|------------------------------------------------------------------------------------------------|------|------|----------|-----------------------------|
| Internal Resistance (Input)      | $R_d$          | $I_C = 5\text{mA}$                                                                             | 450  | —    | 900      | $\Omega$                    |
| Residual Voltage Ratio           | $V_{HO} / V_H$ | $I_C = 5\text{mA}$ , $B = 0 / B = 0.1\text{T}$                                                 | —    | —    | $\pm 10$ | %                           |
| Hall Voltage (Note 1)            | $V_H$          | $I_C = 5\text{mA}$ , $B = 0.1\text{T}$                                                         | 55   | —    | 140      | mV                          |
| Temperature Coefficient (Note 2) | $V_{HT}$       | $I_C = 5\text{mA}$ , $B = 0.1\text{T}$<br>$T_1 = 25^\circ\text{C}$ , $T_a = 125^\circ\text{C}$ | —    | —    | -0.06    | % / $^\circ\text{C}$        |
| Linearity (Note 3)               | $\Delta K_H$   | $I_C = 5\text{mA}$ , $B_1 = 0.1\text{T}$ , $B_2 = 0.5\text{T}$                                 | —    | —    | 2        | %                           |
| Specific Sensitivity (Note 4)    | $K^*$          | $I_C = 5\text{mA}$ , $B = 0.1\text{T}$                                                         | —    | 27   | —        | $\times 10^{-2} / \text{T}$ |
| Internal Resistance (Output)     | $R_{OUT}$      | $I_C = 5\text{mA}$                                                                             | 580  | —    | 1350     | $\Omega$                    |

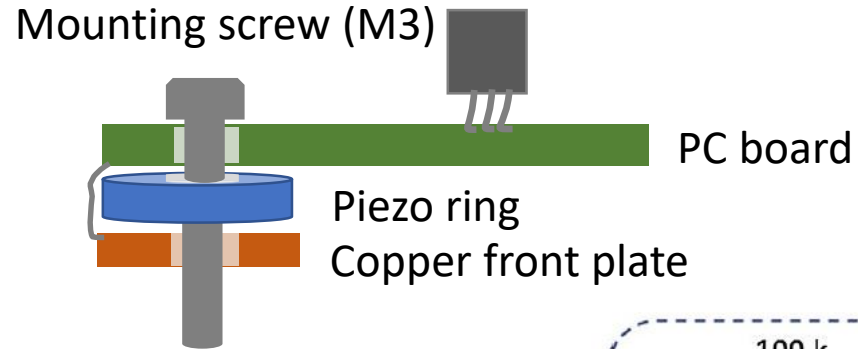
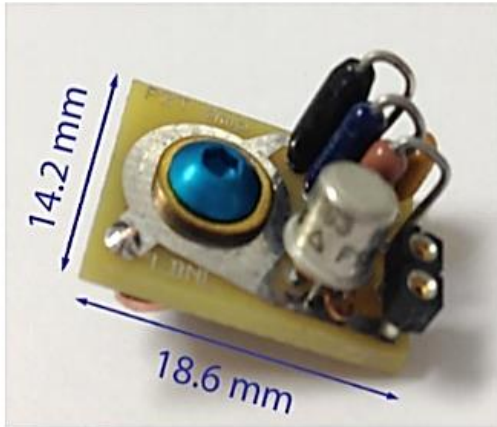
GaAs planar ion-implanted Hall effect sensors (made for automotive applications) are excellent performers at cryogenic temperature.



Current re-distribution along HTS CORC® cable terminals as function of time during quench development measured with the Hall array

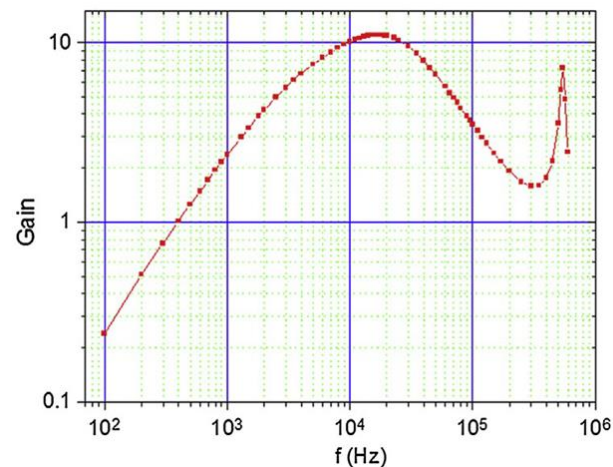
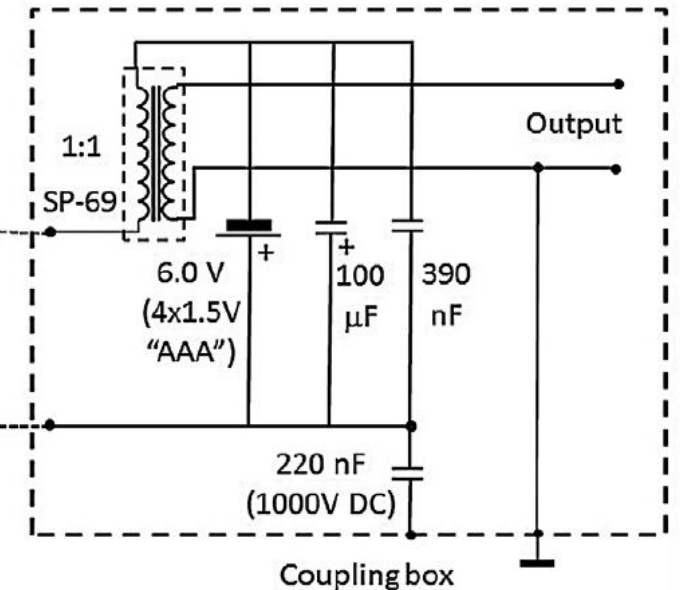
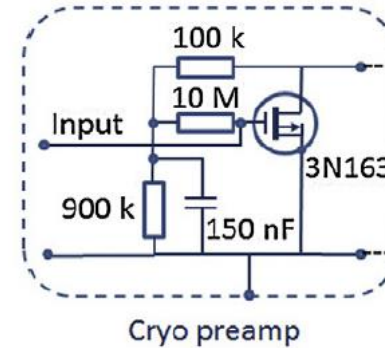
*CORC® cable terminations with integrated Hall arrays for quench detection”, R. Teyber et al., Supercond. Sci.Technol., 33, (2020)*

# Acoustic emission sensor



A robust “workhorse” sensor developed and used at LBL on most of our magnets. It is now also used by other labs (FNAL BNL, CERN) and various projects.

- Based on a single P-channel enhancement mode MOSFET
- Uses only 2 wires (twisted pair or coax)
- Bandwidth is ~300 kHz
- Power consumption is ~ 25 mW
- 2-3 mV rms of noise

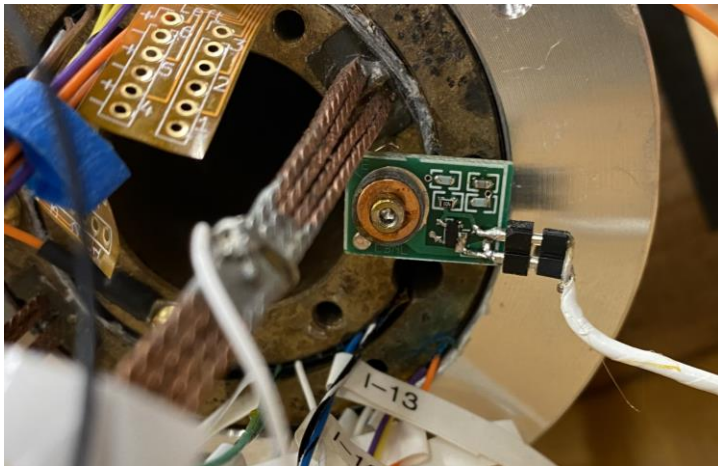


“Acoustic emission during quench training of superconducting accelerator magnets”, M. Marchevsky, G. Sabbi, H. Bajas, S. Gourlay, Cryogenics 69, 50–57 (2015)

# Latest 2-wire sensor re-design

- 2/3 the size of the original sensor
- M2 mounting screw
- < 5 mm thickness (including the piezo-element)
- Better high-frequency response

Same 2-wire interfacing, fully compatible with old interface and powering hardware

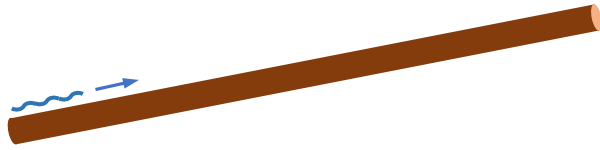


Various supporting structures for AE sensors

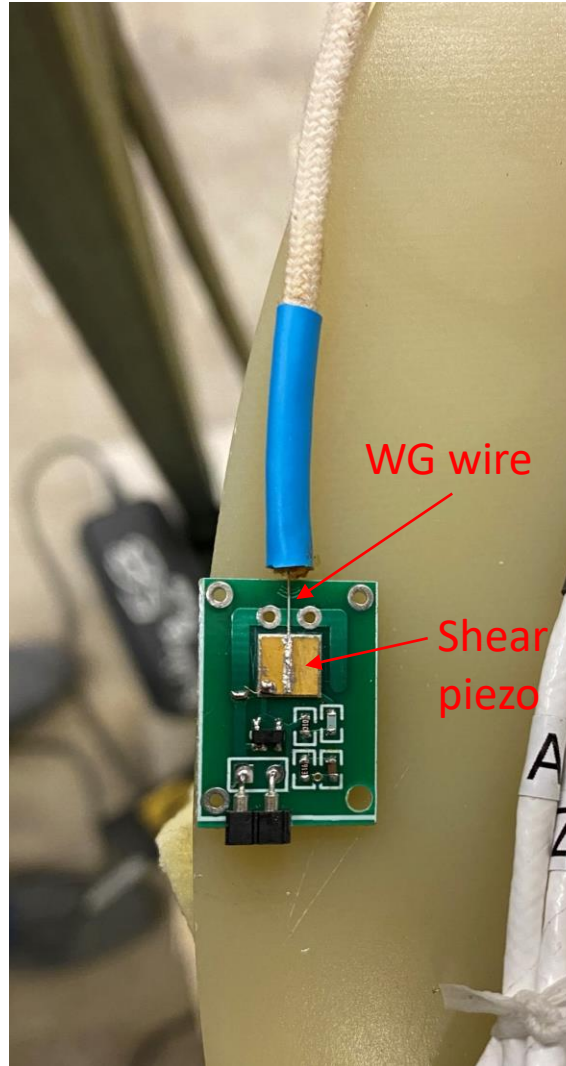
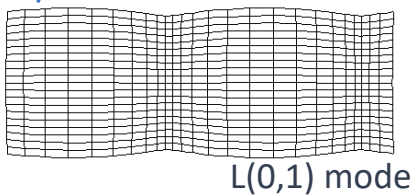
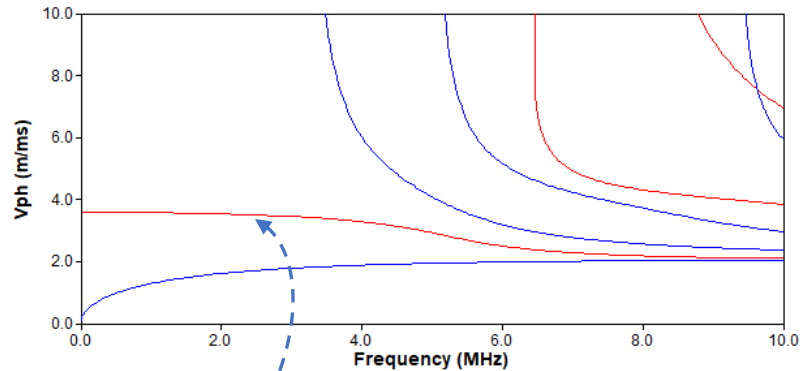


*R. Teyber, M. Maruszewski*

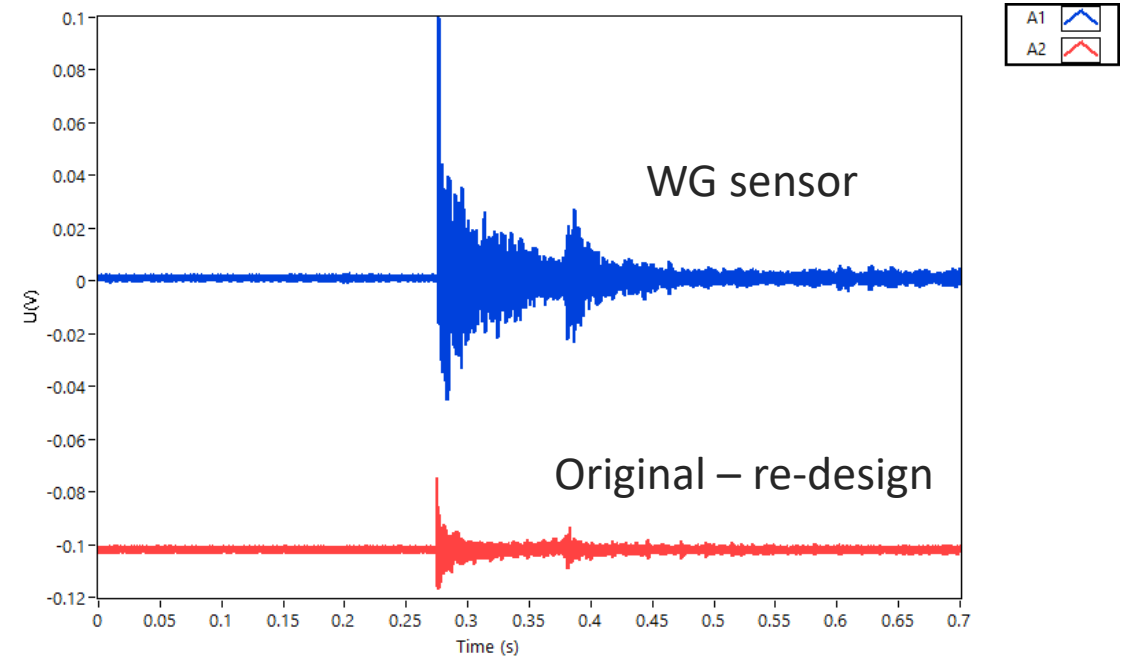
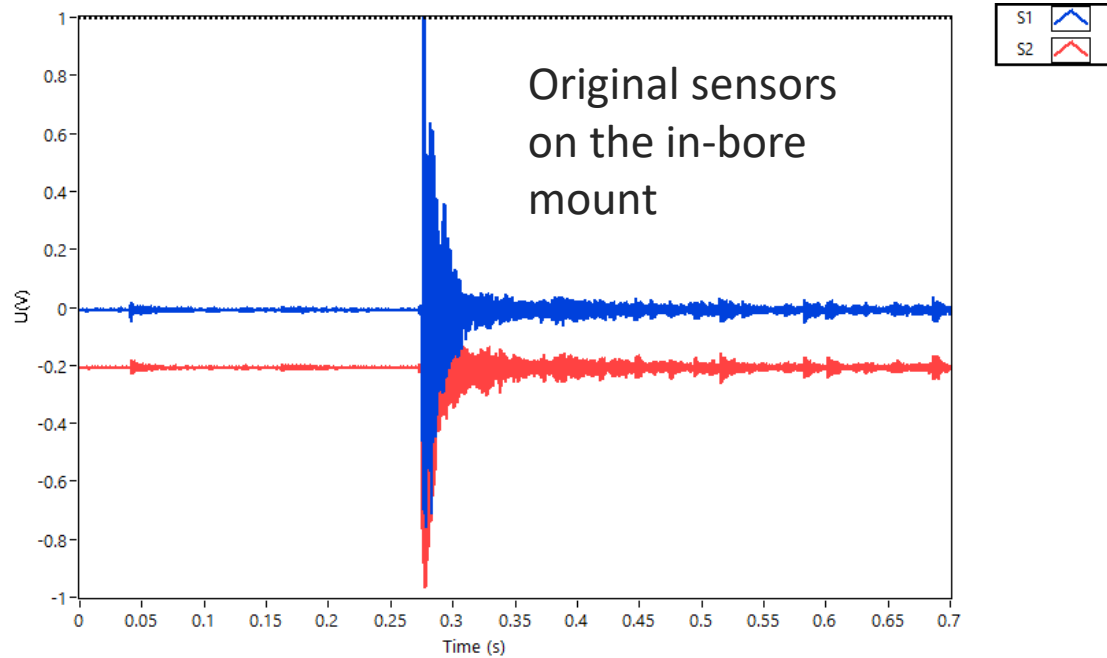
# Waveguide acoustic sensors



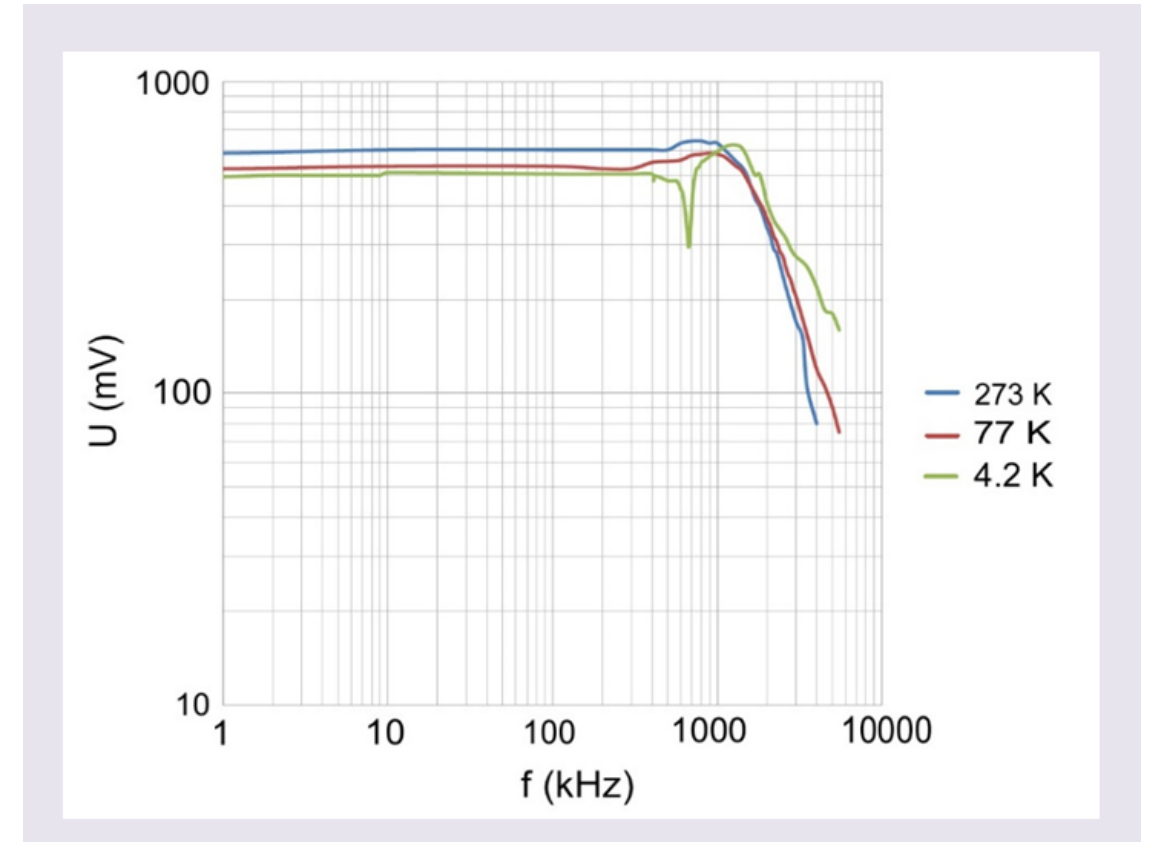
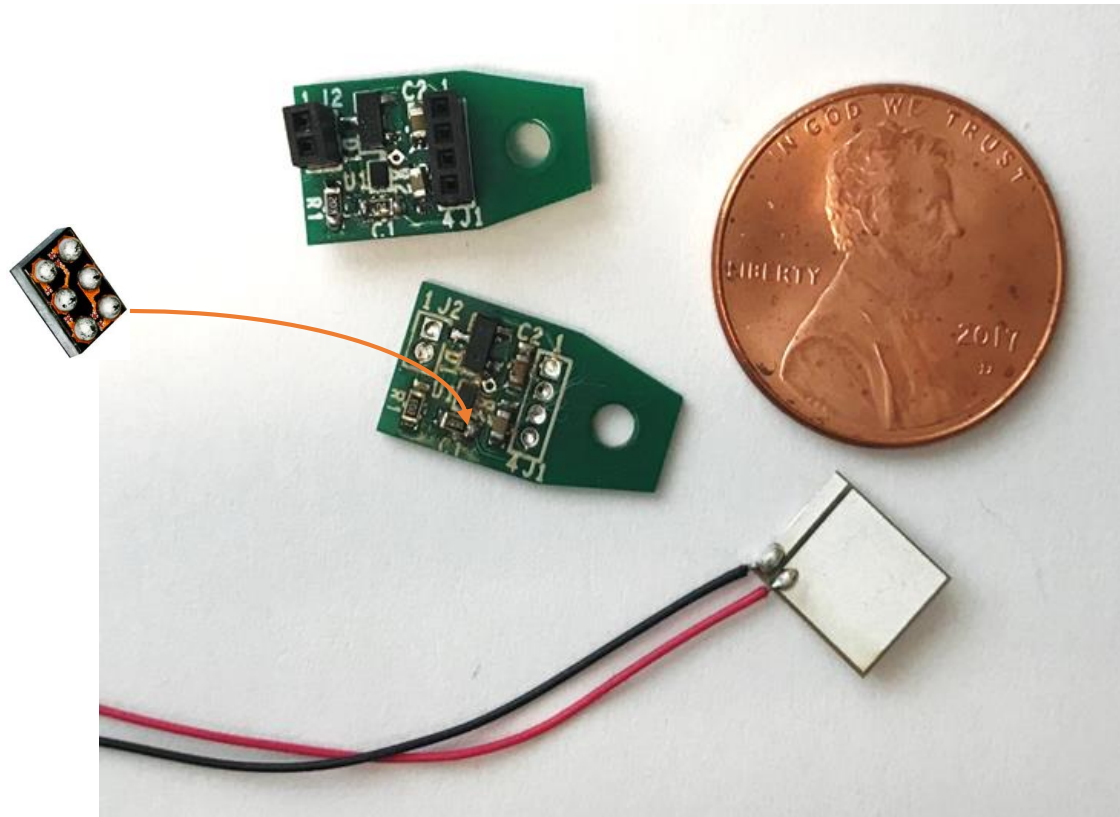
Dispersion plot for traveling acoustic waves in a 0.4 mm diam. brass rod



- The entire sensor is one low-profile soldered board, including the piezo.
- It can be installed away from the magnet; acoustic signal is fed from the magnet by a waveguide wire
- Enables multiple sensors being integrated in a single board, probing specific locations inside the magnet that otherwise are impossible to reach with standard diagnostics



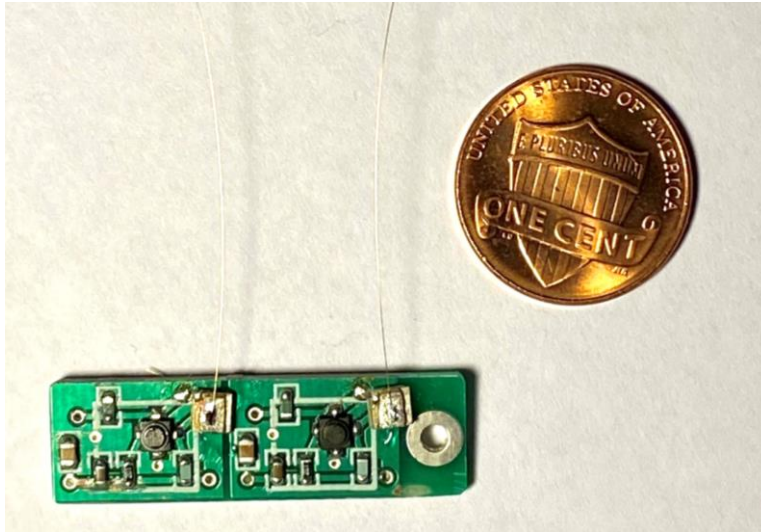
Quench in Nb<sub>3</sub>Sn CCT Subscale 3 dipole monitored with the old and new style acoustic sensors



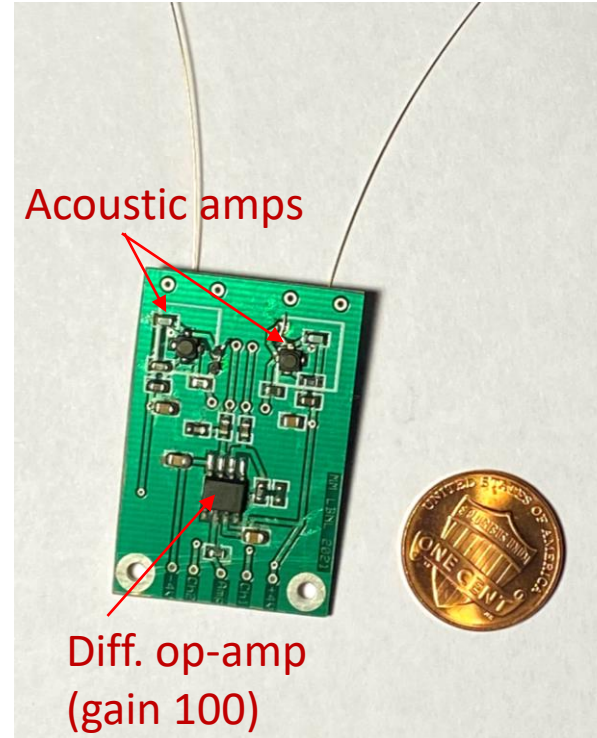
- Based on ultra-low-power Maxim Integrated MAX44290 chip
- Power consumption at 4.2 K is ~15 mW with +/- 3V rail to rail output
- High impedance ( $> 1 \text{ M}\Omega$ ), diode-protected input
- Excellent noise performance
- Flat frequency response in 0-1 MHz range

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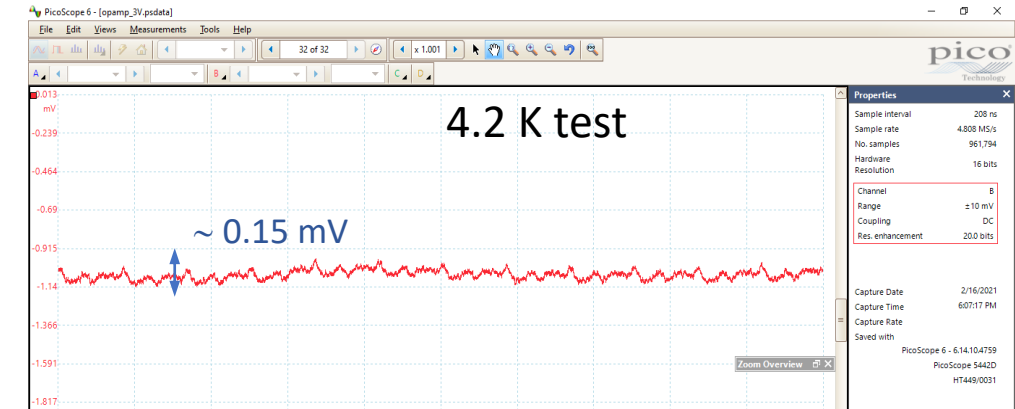
# “Acoustic tap” boards



Waveguide  
acoustic sensors based on GaAs FETs



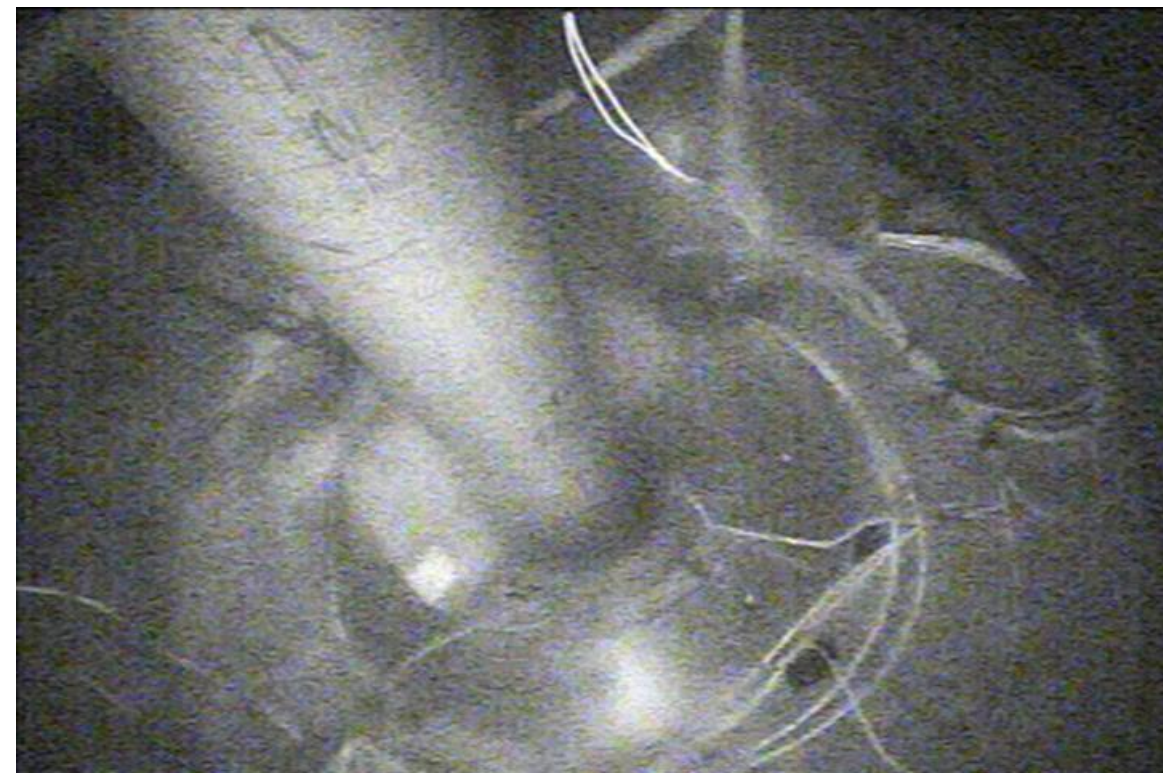
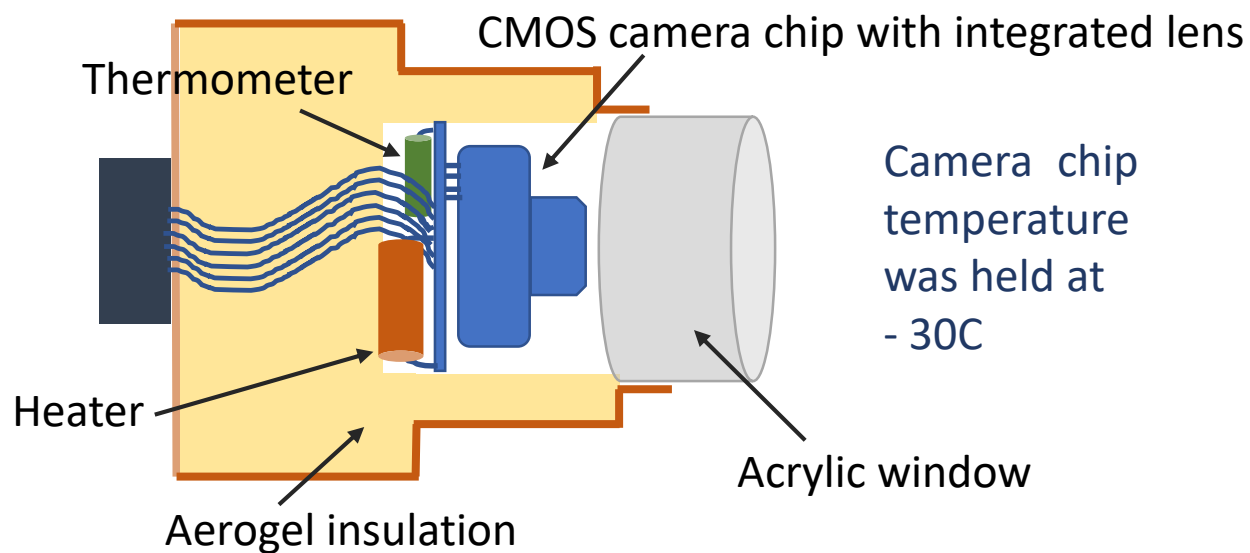
“Universal tap” board: two  
acoustic amplifiers  
combined with a differential  
amplifier based on SiGe  
technology



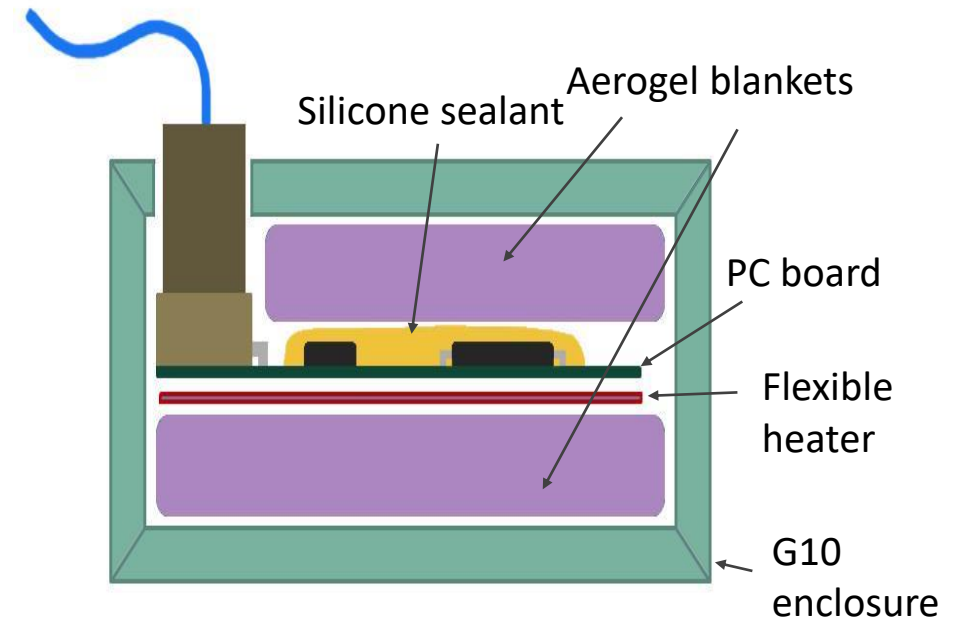
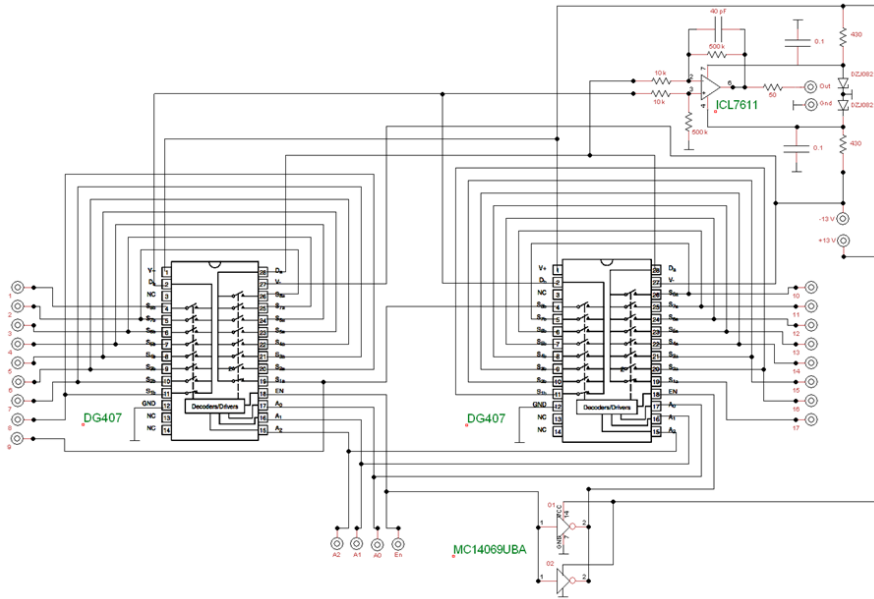
- Extremely low noise ( $< 1 \text{ nV}/\sqrt{\text{Hz}}$  at 1 MHz), uniform performance 300 K- $\rightarrow$  4.2 K
- Ultra wide bandwidth, limited by the piezo-transducer Single-ended and differential amplification possible
- $50 \Omega$  output

- Simultaneous measurement of differential voltages and acoustic emissions can be achieved with a single pair of taps

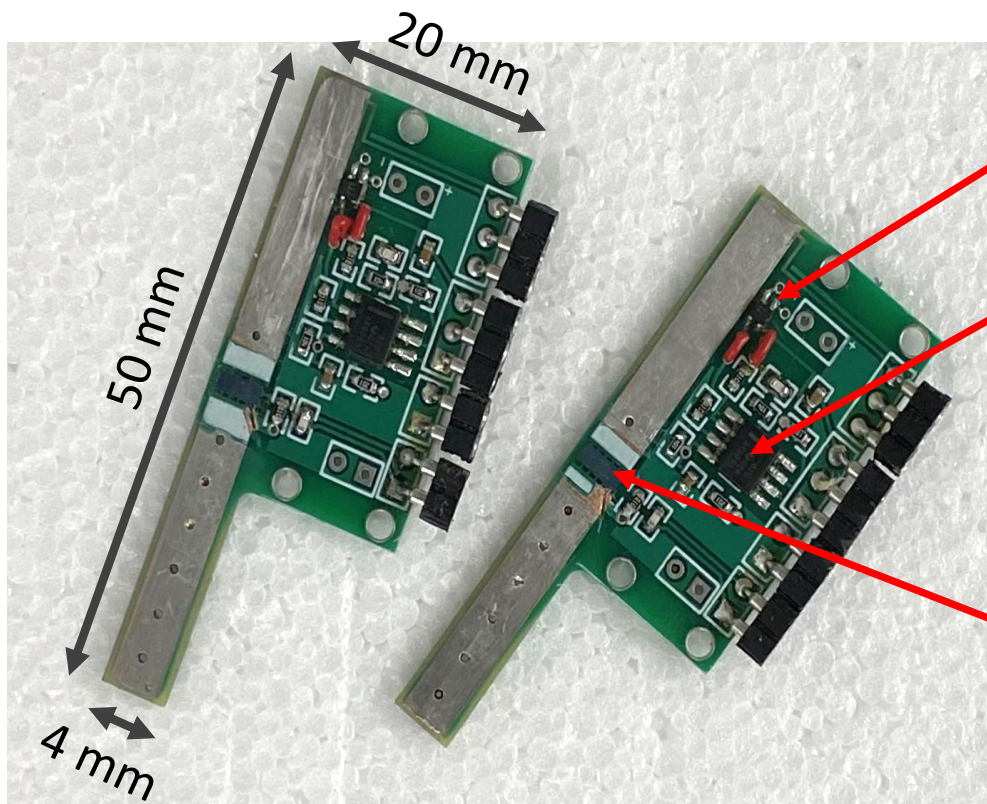
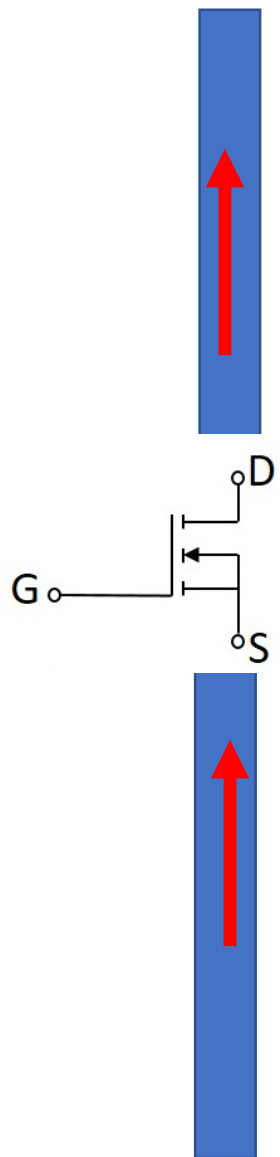
# “Video calorimetry” enabling quick identification of heat sources in the magnet



- CCT3 magnet quenching at ~11 kA
- One can hear the quench occurring in the magnet (“hissing” sound) followed by a slight increase in boiling
- ~2 s later helium bath comes to violent boiling and liquid is propelled upwards along the bore tube.



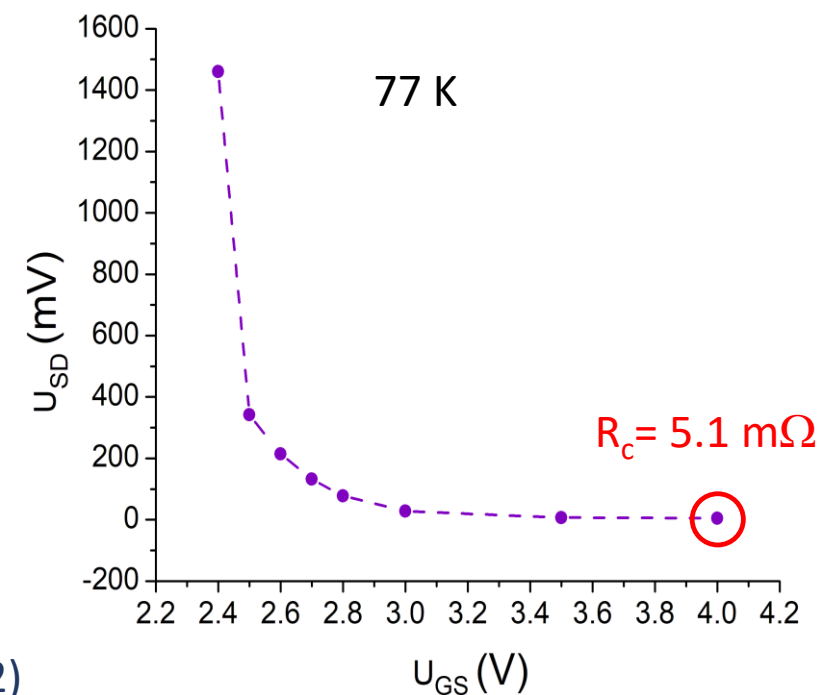
- Two 8-channel DG407 analog multiplexers are commutating 16 differential inputs to a gain x50 amplifier built using ICL7611 op-amp.
- Reliable operation has been confirmed down to 30 K, with switching rates up to 60 kHz/ch limited by the performance of control software. At lower temperatures the **DG407** ICs were no longer responding to control voltages, but the operation restored back to normal at above 30 K.
- To extend low-temperature functionality, the board was sandwiched with a flexible Kapton sheet incorporating a 50-micon thick stainless heater ( $R = 9 \Omega$ ) and two Aerogel blankets inside a G10 box enclosure. With only 0.3 A dc current in the heater the board temperature can be raised above 30 K without having any notable impact on the helium boil-off rate



Hall sensor

Op-amp

Power  
NMOS



- Can drive up to 50 A (room temp, over 100 A expected in LN2)
- Used for quench detection and protection, imaging studies with HTS conductors

- Synergistic approach to data acquisition and pre-processing. Combining various magnet sensors together with real-time digitizer and pre-processors. A cryogenic magnet “neural system”.
- Integration with magnet, structural elements and cryogenic infrastructure. “Smart” terminals, functional supports, etc.
- Cross-integration with other technologies (optical fibers, RF)
- Cryo-electronics status changes from being a “novelty” in magnet diagnostics to becoming a mainstream approach, essential part of future magnet diagnostic systems.